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AMRL-TR-77-7





BIOMECHANICS AND ANTHROPOMETRY FOR COCKPIT AND EQUIPMENT DESIGN

UNIVERSITY OF DAYTON RESEARCH INSTITUTE BIOENGINEERING DIVISION DAYTON, OHIO 45469

March 1976



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FOR THE COMMANDER

CHARLES BATES, JR.

Chief

Human Engineering Division

Aerospace Medical Research Laboratory

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

This report describes enhancements made to the AMRL COMBIMAN (COMputerized Blomechanical MAN-model) program in the areas of man-model link-system and enfleshment characteristics, and in the area of additional functions or options made available to the user of the interactive graphics computer program of COMBIMAN. These new functions include obtaining hard-copy plots of the man-model and workstation as displayed on the Cathode Ray Tube (CRT),

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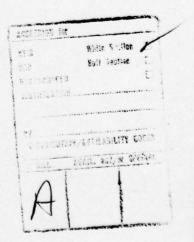
and obtaining visibility plots of the workstation boundary.

The report also documents technical procedures followed in readying the AMRL HERCULES (Human Engineering Research to Cull Efficient Strength) Lab for measuring strength capabilities of seated operators, and the procedures established for running the subjects and gathering the data. The last area covered in this report is the development of programs and the manipulation of anthropometric data used in the analysis of human size variability data. This includes preliminary documentation for the Multiple Bivariate Plotting program, and the procedure established in standardizing the AMRL Data Bank Library Computer Programs, and the AMRL Data Bank Tape Library.

SUMMARY

This report describes the engineering services performed by the University of Dayton Research Institute (UDRI) to provide the Aerospace Medical Research Laboratory (AMRL) with biomechanic and anthropometric data in a form readily and clearly interpretable by design engineers. The ultimate use of the data will be in developing specifications and standards for cockpit geometries of advanced aircraft and personal-protective equipment. The primary effort was to modify, maintain, validate, and document computer programs for guiding the design and evaluation of cockpit geometries and to present, in standard format, the computer programs designed for analyses of military anthropometric data. These are required for the design of workstations, personal-protective equipment, and human analogs. The secondary effort was to provide engineering and research support to studies describing strength characteristics of AF personnel.

The work described in this report is a direct outgrowth and represents a continuation of the development and documentation of AMRL's COMputerized Blomechanical MAN-model (COMBIMAN) program. It also describes the continuation of the extensive work in developing and standardizing computer programs designed for the efficient analysis of presentation of anthropometric data for guiding the design of AF systems and equipment.



PREFACE

This report documents research performed by personnel of the University of Dayton Research Institute (UDRI) for USAF Contract F33615-75-C-5092, entitled "Biomechanics and Anthropometry for Cockpit and Equipment Design". The government work unit number for this contract is 71840824. The contract was monitored by Dr. Joe W. McDaniel, of the Crew Station Integration Branch, Human Engineering Division, Aerospace Medical Research Laboratory, Wright-Patterson Air Force Base, Ohio. The principal investigator on the contract was Ms. Susan M. Evans, while Paul E. Kikta provided programming support, and Martin J. Himes provided technical support. David Nearing provided programming support for program RANDM, documented in Section 3.

The research documented in this report was performed in conjunction with personnel of the Crew Station Integration Branch. In particular, Drs. Joe McDaniel and Kenneth Kennedy provided valuable data and equations used in the generation of the COMBIMAN man-model. The link system presently used in COMBIMAN is the result of research performed by personnel in the Crew Station Integration Branch (AMRL/HED), in particular Dr. Kenneth W. Kennedy. Mr. Charles Clauser directed much of the effort involving the bivariate program, the standardization of the AMRL Anthropometric Data Base, and the biostereometric program. Dr. H. E. Krause, formerly of UDRI, also participated in the development of the enfleshment ellipsoids about the COMBIMAN man-model. The authors gratefully acknowledge his assistance, as well as that of the staff of the UDRI.

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SECTION 1 INTRODUCTION

This report covers the enhancements made to the Aerospace Medical Research Laboratory (AMRL) COMBIMAN program, the efforts to standardize the AMRL Anthropometric Data Bank, and the research support provided for studies describing the strength characteristics of AF personnel.

The work documented in this report is a direct outgrowth and represents a continuation of the development and documentation of AMRL's COMputerized Blomechanical MAN-model (COMBIMAN) program. The COMBIMAN program has been developed to provide the workstation engineer with an interactive graphics program to be used in the design and evaluation of aircraft cockpits. This report describes the procedures developed for the generation of the link system and enfleshment of the COMBIMAN man-model. It also documents features which enable the user to obtain visibility plots and hard copy plots of the man-model and workstation configurations.

This report also documents the continuing effort in developing and standardizing computer programs designed for the efficient analyses of anthropometric data for guiding the design of AF systems and equipment. In particular it describes the computer program developed to plot multiple survey bivariate tables, the research performed on AMRL-supplied biostereometric data, and the standardization effort dealing with the programs and the anthropometric survey data tapes of the AMRL Anthropometric Data Bank.

SECTION 2

FURTHER DEVELOPMENT OF THE COMBIMAN PROGRAM

This section documents the continued development of AMRL COMBIMAN (COMputerized Blomechanical MAN-model) program, as performed by UDRI personnel during this contract period. The three primary areas covered in this section are the enfleshment procedures established for the man-model, the plot program developed to generate hard copy plots of the man-model and workstation as displayed on the IBM 2250-3 Cathode Ray Tube, and the on-line generation of visibility plots. Another area of development which will not be documented here is the COMBIMAN User's Guide (Reference 1), written during this contract period. It reflects the operational status of the COMBIMAN programs as of 1 November 1976.

2.1 ENFLESHMENT OF THE MAN-MODEL

The man-model used in COMBIMAN is based on a 33-link skeletal system. Each of these links connects major points of rotation of the body segments. The model is constructed by the interactive graphics program of COMBIMAN in three stages. The first stage is the generation of the link system of the model. The second stage involves the definition of the enfleshment ellipsoids about the link system joints. The third stage is the connection of the elliptical projections with tangent lines.

2.1.1 Generating the Link System

Although 33 links are defined for the man-model, two of these links are positioning links, and are used to provide a common reference between the seat reference point of the model and the workspace. The links system is constructed by adding links together to form a link chain, starting with the link at the seat reference point (SRP). As each link is positioned, the link end point, or joint location, is defined in terms of a position vector,

with respect to the SRP. The major points of rotation of the body segments are shown in a side view of the model in Figure 1. Work of the Aerospace Medical Research Laboratory (AMRL) with two dimensional drawing board manikins formed the foundation for the three dimensional link system of the COMBIMAN model. AMRL data have been used in defining relationships between measurable anthropometric surface dimensions and difficult to measure internal link lengths, and in defining the range of values for transformation or Euler-type angles used to position the links.

When using the COMBIMAN interactive graphics program CBM04, the user has the ability to vary the proportions of the model to suite the needs of the application. The user may supply values as dimensions or percentiles for a variable number of anthropometric surface dimensions, or may insert the internal link lengths directly. To alter the position of the model, the user changes any of the values for the Euler-type angles available for each link. More information on the procedures for altering the dimensions of the model is given in the COMBIMAN User's Guide - (Reference1).

At the present time the equations used to establish the internal link lengths have not been validated against real life data. This is to be done in the upcoming contract period. Because they have not been validated, actual equations based on AMRL supplied data will not be presented in this report.

In assembling the individual links called L_i to establish joint locations in three dimensional space, the length and the three-dimensional Euler-type angles of a particular link are used, along with the three dimensional coordinate of the previous link, L_{i-1} , and the product of the transformation matrices which positioned L_{i-1} . The three Euler-type angles used for each link correspond to the three rotations of the coordinate axis of the system about link L_i to establish its location relative to link L_{i-1} . If all the Euler angles between adjacent links are specified, the geometric configuration of the man-model is specified. A more detailed description of the use

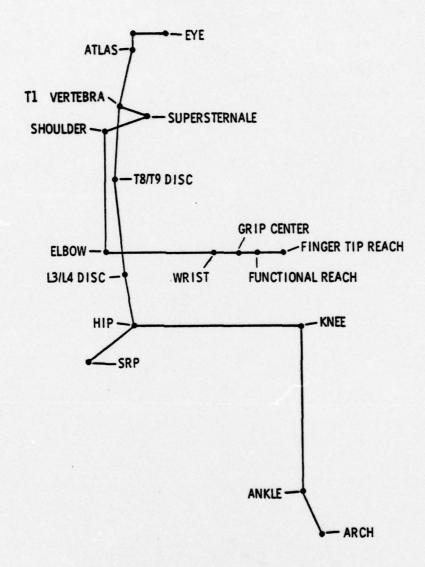


Figure 1. Side View of COMBIMAN Link System (Reference 2).

of transformation matrices and the establishment of joint locations, see Chapter 2 in Reference 3. This technique of positioning links places realistic limitations on the range of mobility of each joint and permits the repositioning of the distal link, L_i, by movement of a proximal link, say L_{i-1}.

2.1.2 Enfleshment Ellipsoids

The enfleshment, or addition of volume about the links, of the stick man-model to produce a realistic and anthropometrically correct manmodel starts with the joints of the stick man-model. The joint at the distal end of each link is surrounded with an ellipsoid (three dimensional ellipse) for this purpose, as shown for a side view of the model in Figure 2. Figure 3 shows a system of coordinates for a joint at the distal end of the link L_{T_i} . This is known as the "link's system of coordinates." It is permanently attached to the end of the link, and moves with it in space. It is used to define the orientation of the next distal link which is attached to the joint.

The size and shape of an ellipsoid is defined by the dimensions of the semiaxes a, b, and c in Figure 3. These dimensions are based on body surface and mass dimensions, and derived from equations supplied by personnel of AMRL/HED. The semiaxes dimensions for each joint correspond to the height, width and breadth surface dimensions at that joint.

The position of the ellipsoid in space is determined in relation to the individual link's system of coordinates. The dimensions α , β , and γ in Figure 3 specify the distances by which the center of the ellipsoid is offset from the origin of system of coordinates in the x, y, and z directions respectively. The ellipsoid is centered at the origin of the system of coordinates, and therefore about the center of rotation, if $\alpha = \beta = \gamma = 0$.

The angular alignment of the ellipsoid is another necessary quantity to define its position. The y axes of the links' system of coordinates of the present stick-man model have been aligned with the major axis of rotation of the joint. The semiaxis b of the ellipsoid is aligned with this major

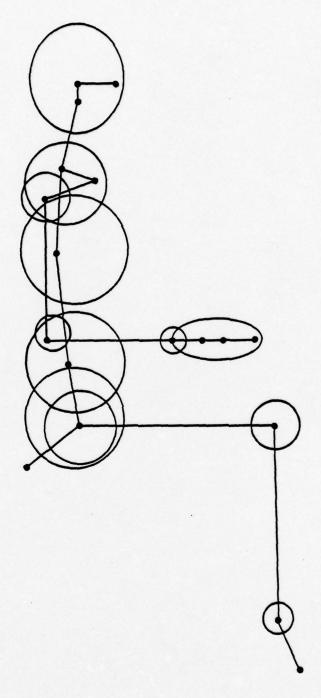


Figure 2. Side View of COMBIMAN With Enfleshment Ellipses (Reference 2).

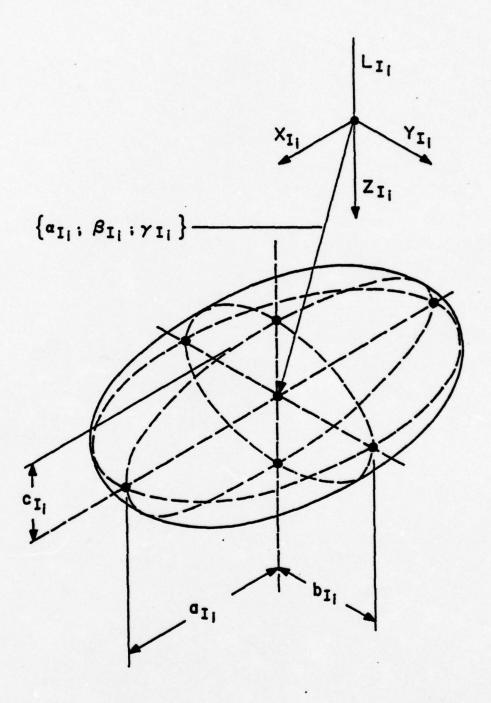


Figure 3. Ellipsoid Surrounding the Distal Joint of Link L.

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axis of rotation. All ellipsoid axes are parallel to the axes of the link system of coordinates. This alignment produces a realistic contour of highly flexible joints at any degree of joint flexion or extension. The semiaxes a and c will have identical dimensions in most flexible joints. The cross sectional area of the ellipsoid in planes parallel to the z-x plane is thus circular. This enables the ellipsoid to function like a ball joint and to maintain anthropometrically realistic dimension in several directions.

The COMBIMAN man-model is displayed by projecting two orthogonal views on a cathode ray tube screen. The ellipsoids surrounding the joints are also projected into the screen. These projections are ellipses and are identical to the shadow of the ellipsoids produced by a source of parallel light perpendicular to the viewing screen. The man-model can be rotated and magnified or reduced within the viewing area. Any such manipulation changes the shape and/or size of the projected man-model. Any such manipulation will also change the shape and size of the shadow of a given ellipsoid on the cathode ray tube screen. The essence of the joint enfleshment stage is the definition of the projected ellipses under all conditions of body positions and viewing angles.

The projected contour of the ellipsoid onto a screen is identical to the crest (visible outer boundary) of the ellipsoid. The equations which have been developed by UDRI in conjunction with AMRL personnel are defined in detail in Section 2 of "The COMBIMAN Enfleshment Procedure and Expanded Joint Mobility Analysis", published as UDRI-TR-76-18, by the University of Dayton Research Institute in September, 1976.

The equations which are used to establish the lengths of the semiaxes a, b, and c for each joint, have not yet been validated against actual subject data. This, like the validation of the data used in stage one, is a key task to be accomplished during the next contract period.

2.1.3 Tangent Line Connectors

The last stage of the man-model generation is the connection of the elliptical contours of adjacent joints with tangent lines. This is done separately for all the contours in each viewing plane. Figure 4 shows a side view of the model with the tangent lines added. In this figure, unnecessary elliptical outlines have been eliminated. The present COMBIMAN program retains all outlines on the various views.

The equations used to establish the location of the endpoints of the tangent lines were developed by AMRL/HED personnel, in particular Dr. Joe McDaniel. The procedure used requires two sets of points which define the contours of two ellipses, each around a point of origin, with a link connecting them. One of the points of origin, and the set of points about it will be called proximal, and the other point will be called distal. From a point along the line passing thru the proximal and distal points, but beyond the proximal point, compute the slope of lines connecting this new point with each of the points on the distal ellipse. Locate the minimum and maximum slopes. From the point used in defining the maximum slope to the proximal projection, calculate the slopes to each point on the distal projection, and locate the minimum slope. From the first point used to define the first maximum slope, calculate the slope to each point on the proximal projection, and find the minimum slope. From the point used in defining this last minimum slope on the proximal projection, calculate the slopes to each point of the distal projection, and locate the maximum slope. A more detailed explanation of this procedure is shown in the flowchart in Figure 5.

The points which are located in steps 2 and 3, and 4 and 5 in Figure 5 define the endpoints of two tangent lines connecting adjacent links for one view of the model. This procedure is repeated for each combination of elliptical projections of adjacent links, for each view of the model.

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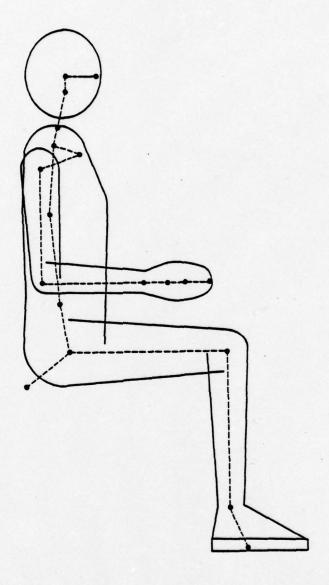


Figure 4. Side View of COMBIMAN With Tangent Lines (Reference 2).

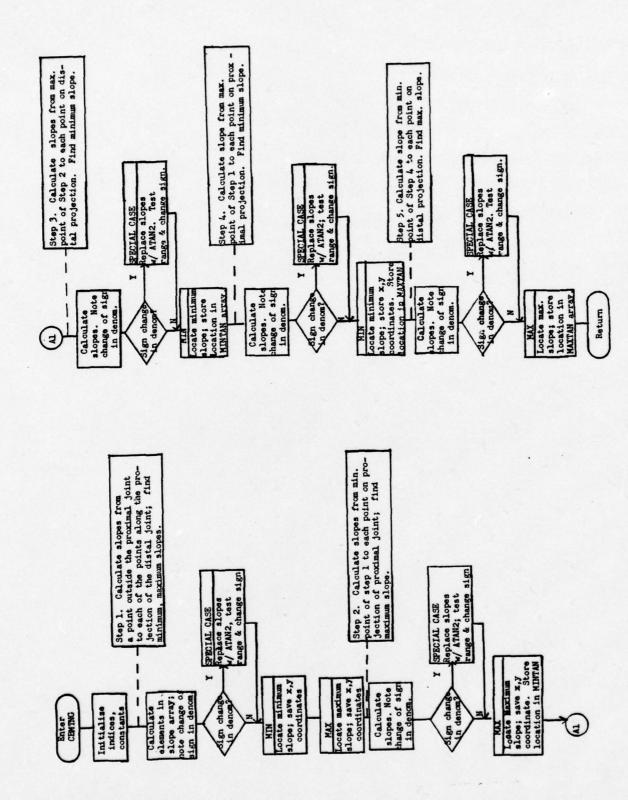


Figure 5. Flow of Tangent Line Subroutine.

Because of the nature of certain adjacent links, the enfleshment ellipses may appear to be concentric at certain viewing angles. Eventually, the tangent line subroutine will be able to detect this, and not calculate tangent line endpoints. At the present time, however, it attempts to calculate tangent lines, and often generates unusual results. An example of concentric ellipses in the side view is shown in Figure 6. The "tangent lines" connecting the MID-HIP projection and the RIGHT UPPER THIGH projection lay within the outer projection, creating unnecessary clutter on the display for the viewer.

The subroutine of the interactive graphics program CBM04, which issues the graphics orders to plot the man-model on the IBM 2250 CRT, uses the x, y, and z coordinates which define the endpoints of each link with respect to the SRP of the model. It uses the coordinates two at a time, however, to project the X-Z (side) plane, and the Y-Z (top) plane of the model (giving two orthogonal views). One view is completely generated, combining the link vertex data with the elliptical projection and tangent line coordinates for that view. The generation of and use of data for X-Y (top) plane is optional, but the user may decide to calculate this extra set of projectsions and tangent lines for use in hard copy - plots of the man-model/workspace configuration. The hard copy plots are discussed in the next paragraph.

2.2 PLOT COMBIMAN

In order to obtain hard-copy representations of the man-model and workstation configuration currently being displayed on the IBM 2250 Cathode Ray Tube (CRT), subroutines were developed and added to the COMBIMAN interactive graphics program CBM04 to generate two to three two dimensional plots on the HESS's on-line GOULD electrostatic plotter. The subroutines use the data arrays of three dimensional real world coordinates which are contained in computer memory and which represent the configuration of the link system of the model, the points on the elliptical projections, and the panels of the workstation. The subroutines also use data on the range of

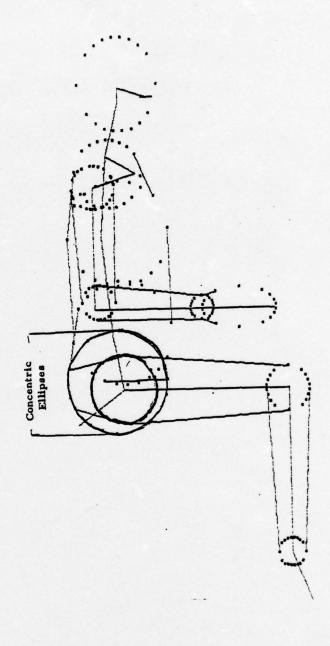


Figure 6. Side View of Model With Concentric Ellipses at Mid-Hip and Right Hip Identified.

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x, y, and z-values contained in the arrays. These data were originally calculated by the subroutine which scales coordinate data to fit in the display area of the CRT and issues the graphics orders to generate the display. The range-data used include the maximum x, y, and z-coordinates found among the points, the ranges over x, y, and z-values, and the maximum of the three ranges.

2.2.1 Data Preparation

The user of the interactive graphics program has two options for specifying the size of the plots to be generated. The user can specify a scale factor from 0. to 1. or can omit any scale factor. For specific instructions on entering scale factors, see Paragraph 2.2.8 of the User's Guide for the Programs of COMBIMAN, AMRL-TR-76-117 (Reference 1). If no scale factor was supplied, the subroutine uses a factor which will scale the coordinates so as to make optimum use of a nine by nine inch plot area for each view. Once a scale factor has been established, the x-coordinates in the data arrays are scaled as follows:

NEWX = (R-WX - XMAX + (MAXDIF - XDIF)/2.0) * SCALE

where: NEWX is the scaled x-coordinate value

R-WX is the unscaled x-coordinate value in the COMBIMAN

base system of coordinates

XMAX is the maximum x-coordinate of all the coordinates

in the x-coordinate data arrays

MAXDIF is the maximum range of coordinates in either the

x, y, or z direction

XDIF is the difference between the minimum x-coordinate

value and the maximum x-coordinate value

SCALE is the available scale factor

The y and z values are scaled similarly, using the following equations.

NEWY = (R-WY - YMAX - (MAXDIF - YDIF)/2.0) * SCALE

and

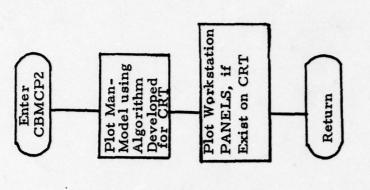
NEWZ = (R-WZ - ZMAX - (MAXDIF - ZDIF)/2.0) * SCALE

2.2.2 Plotting

Before the plots of the model and workstation are generated, the main subroutine prints the names of the anthropometric and regression survey used in generating the model, and the name of the workstation used. if one is being used on the plotter. From two to three plots are then generated of the two dimensional views of the model and workstation. The two views which will always be generated are of the X-Z plane and the Y-Z plane. If, prior to selecting the plot COMBIMAN function, the user selected State Switch 11, a third view of the X-Y plane will also be generated. A detailed description on setting State Switches is given in Paragraph 2.2.22 of the User's Guide (Reference 1). A general flow diagram of this main subroutine is shown in Figure 7. The actual plots are generated in a second plotter subroutine which calls the routines of the GOULD Plotter Package (see Reference 4), and plots the link system of the model, enfleshment projections, and the workstation panels for the view in question. A flow diagram of this second subroutine is shown in Figure 8. A complete plot, with three views of the model and workstation is shown in Figure 9.

2.3 GROUND VISIBILITY PLOTS

A subroutine has been added to the COMBIMAN interactive graphics program which enables the user to obtain ground visibility plots. The routine uses the eye location of the man-model in place of a camera lens, as used in AMRL-TR-69-123 (see Reference 5). The routine also provides the user with a cockpit visibility record. The boundary coordinates of objects to be plotted are obtained from engineering drawings of typical aircraft cockpits. The boundary coordinates, in the aircraft system, are read into the subroutine and first converted to the seat reference point coordinate system of the man-



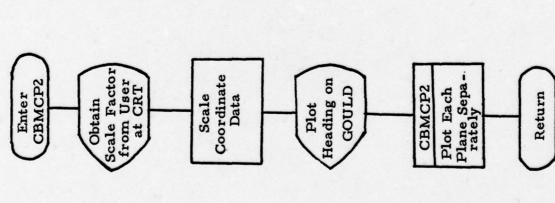


Figure 7. Flow Diagram for Subroutine CBMCP1.

Figure 8. Flow Diagram for Subroutine

CBMCP2.

REGRESS=REGRES01 SURVEY=67SURVEY WKSP= A7E-01.

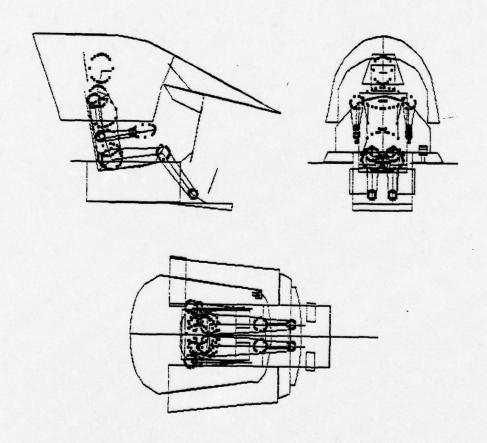


Figure 9. Sample Plot of Man-Model and Workstation from X-Z Y-Z and X-Y Planes.

model, and then to the eye coordinate system of the model, with either the mid-eye, right eye, or left eye point of the man-model being the new origin. The eye point used by the subroutine is determined by the user. The routine then calculates the viewing angle of the model with respect to horizontal and vertical, and uses these angles to establish the cockpit visibility records.

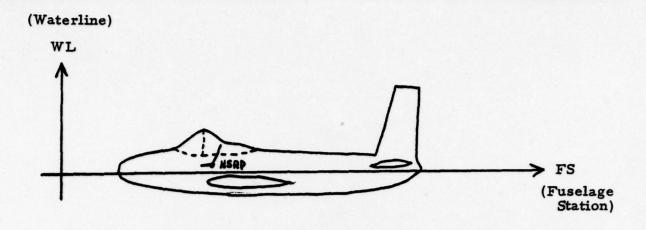
The Visibility Plot subroutine calculates the limits of the fields of vision of the present configuration of the model and superimposes these limits over the boundary coordinates of objects of an existing workspace. It then plots them both on an on-line GOULD plotter. At the present time, the workspace which is being used is that for the A7 cockpit.

As the necessary engineering drawings for more workspaces become available, more boundary coordinates can be typed onto computer cards and added to a special disk file and be made available to the user.

2.3.1 Workspace Outline Coordinate Data Input

Data for use by the visibility plot subroutine are originally obtained from engineering drawings. The three dimensional boundary coordinates of objects to be plotted, such as aircraft canopies, windscreens, and other key outlines, are obtained in the aircraft system of coordinates. The orientation of this system is shown in Figure 10. In addition to gathering coordinate data on the key boundaries in the workspace, the location of the neutral seat reference point in the aircraft coordinate system must also be obtained. When collecting points along the boundaries, it should be noted that the greater the number of points supplied to the subroutine, the smoother the plot will be. The maximum number of points allowed for any one boundary is 200.

Once the data are obtained from the engineering drawings, they should be punched onto computer cards using the formats shown in Figure 11. The first card is punched using the format in Figure 11a. This is done once for the complete set of workspace outlines being considered. The first field on the card, NBND, contains the number of boundaries to be contained in this visibility plot. This value is an integer value, and should be right justified in the five



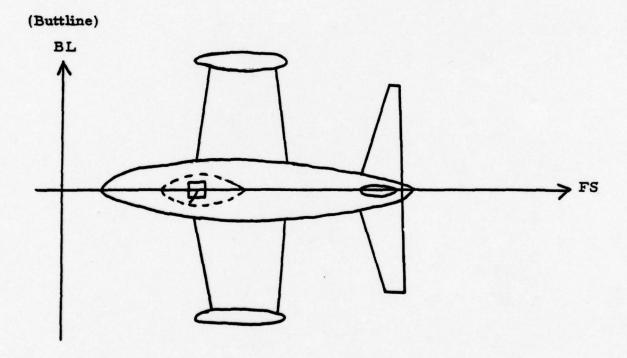


Figure 10. Orientation of Aircraft System of Coordinates.

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AYOUT FORM MULTIPLE-CARD

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	9 9 9	3 9 9 9	1 65 66 67	9 9 9	
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Boundary Points Card Format.

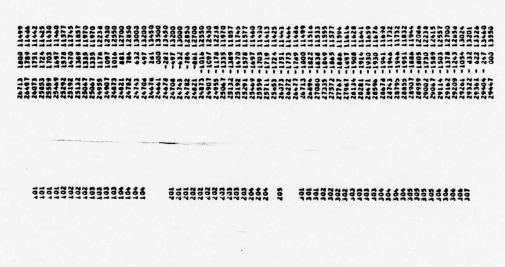
Figure 11. Input Formats for Visibility Plot Subroutine.

digit field. The next three fields (XAC, YAC, ZAC) define the location of the neutral seat reference point in the aircraft system of coordinates. These coordinates are real values and assume a format of F5.3 if no decimal point is supplied by the user. The last three fields of this card define the location of the seat reference point of the COMBIMAN model with respect to the neutral seat reference point of the aircraft. At the present time these values should be zero or left blank. In the near future they will be obtained from the interactive graphics program CBM04 to reflect variations in the location of the seat with respect to the original neutral seat reference point.

The second and third formats shown in Figure 11 are used for each boundary. The format in Figure 11b contains the number of coordinate sets, NCOORD, which will be used to define this boundary. It is an integer value, and should be right justified in the five digit field. This card also contains an alphanumeric name for the boundary in field BOUNDARY NAME. The name may not be more than 24 characters long. The format shown in Figure 11c is used to define the three coordinates for each point along the boundary. The three coordinates are to be supplied in the aircraft system, and are typed using a F6.2 format. Sample coordinate data for the A7 cockpit is shown in Figure 12. The workspace is defined in terms of three configurations, the Front Bottom Windscreen, the Front Top Windscreen, and the Cockpit Canopy Clearline.

Once all the data have been punched onto computer cards, they are written onto a disk file for use by the interactive graphics program CBM04. The Job Control Cards (JCL) for accomplishing this are shown in Figure 13. The first outlined area in Figure 13 lists the JCL needed to call an IBM utility "IEHPROGM" which scratches any dataset containing workspace boundary data which may exist on disk. The second outline area shows the JCL needed to call the IBM utility "IEBGENER" and create a new dataset called "SME. VISDATA" which will contain the boundary coordinate data available on cards. The third outlined area lists the JCL used to call the IBM utility "IEBGENER"

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Figure 12. Punched Data for A7 Cockpit Boundary.

```
//VISFILE JOB (UDR807, KO), EVANS, MSGLEVEL=1
 /SCRATCH EXEC PGM=IEHPROGM
//SYSPRINT DO DUMMY
                                                             1
//PUBLIC DD VOL=SER=PUBLIC, UNIT=3330, DISP=OLD
/SYSIN DD *
 SCRATCH DSNAME=SME.VISDATA, VOL=3330=PUBLIC
//RECRT EXEC PGM=IEBGENER
//SYSUT2 DD DSN=SME.VISDATA,DISP=(NEW,CATLG),UNIT=SYSDA,
         VOL=SER=PUBLIC, SPACE=(1600,(10,5),RLSE),
         DC8=(LRECL=80, RECFM=FB, BLKSIZE=1600, DSORG=PS)
//SYSPRINT DD SYSOUT=A, DCB=BLKSIZE=121
//SYSIN DD DUMMY
//SYSUT1 DD *
                                                             2
     BOUNDARY OUTLINE CARDS GO HERE
//PRINT EXEC PGM=IEBGENER
//SYSUT1 DD DSN=SME.VISDATA,DISP=OLD
//SYSPRINT DD SYSOUT=A, DCB=BLKSIZE=121
                                                             3
//SYSUT2 DD SYSOUT=A.DCB=BLKSIZE=81
//SYSIN DD DUMMY
```

Figure 13. Job Control Cards Needed to Establish Data Set on Disk Containing Boundary Outlines for Visibility Plots.

again, but this time it prints the contents of the dataset "SME. VISDATA" for verification purposes. A detailed description of each of the IBM utilities used can be found in Reference 6.

Although the boundaries are described separately on computer cards, the individual subsections are automatically recombined before plotting the total visibility plot.

2.3.2 Generating the Vision Angles

The subroutine to generate the visibility plot is activated when the user of the interactive graphics program CBM04 presses the Visibility Plot Function Key (see Reference 1). This subroutine then reads the disk file which has been loaded with workspace boundary coordinates, and stores the available data for the necessary calculations in arrays in memory. If, for some reason, the disk file does not contain any workspace coordinate data, the message "NO DATA AVAILABLE FOR VISIBILITY PLOT ON UNIT 9" will be displayed in the information area of the screen. The routine is ended and the user is asked to depress another function eky.

Once the function key has been depressed and the boundaries read in, the prompting area will display the message "ENTER EYE LOCATION (LINK)". The user must decide on the eye point to be used as a reference for the plots. Possible values are either 8 for Mid-Eye point, 9 for Right Eye point or 10 for the Left Eye point. These values should be typed in, right justified in the eight digit field. Once a valid link number has been specified, the message "PLOTTING" is displayed on the CRT screen.

The routine uses the coordinates which define the endpoint of the Mid-Head link (link 7) and the coordinates of the Mid-Eye point to calculate the angles of sight from horizontal and from vertical. Facing forward and looking straight ahead would be angle of 0° from both horizontal and vertical.

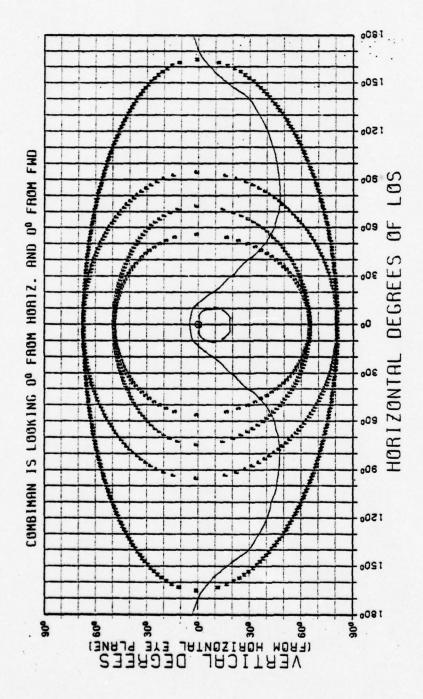


Figure 14. Sample Visibility Plot - Straight Ahead View.

Once the three dimensional coordinates of the boundary have been translated to the eye coordinate system of the model, the subroutine processes the points by iterating over the angular range of the points to determine the intersection of integer angles of horizontal line of sight with the line segment formed by two consecutive points on the workspace boundary. The angular range of points is calculated by the subroutine, and is based on the minimum and maximum horizontal angle of intersection with the workspace boundary being evaluated. The equations which are used to establish the angles of intersection and the coordinates of the boundary at these points were provided by Dr. McDaniel of AMRL.

2.3.3 The Visibility Plot And Printed Output

Figure 14 shows a sample visibility plot with the A7 outline. For this example, the man-model was positioned in a seated erect posutre, looking straight ahead. The vision limits were generated with respect to the angle of sight of the Mid-Eye point (link 8).

The four ellipses on the plot define the limits of various visual fields. The inner most field, plotted with the letter S, defines the field of stereo vision, with both eyes in their normal position. The next field, plotted with the letter F, defines the right and left fixation limits of vision. The third field is plotted with the letter P and defines the limits of peripheral vision associated with the facing forward with respect to the head. The outermost field, plotted with the letter M, defines the maximum peripheral vision limits for the left and right eye. The symbol O defines the normal line-of-sight of the model.

The contour of the workspace boundaries are plotted with respect to the line-of-sight of the man model. As the model's head is shifted from the foward position the workspace boundaries are shifted in the opposite direction. An angle other than zero degrees from the horizontal eye plane of the model causes the boundaries to be raised or lowered based on a positive or negative angle from horizontal. The label indicating degrees on the vertical axis is

shifted in increments of multiples of ten degrees. This increment is calculated by dividing the angle from horizontal by 10., truncating this quotient to the nearest whole number, and then multiplying this value by 10. The boundaries and the visual limits are shifted slightly, so that value obtained with respect to the vertical axis is always labeled with angles which are multiples of 10. A sample visibility plot which was generated using visual angles of -15° from horizontal and 30° from forward is shown in Figure 15.

In addition to generating a hard copy plot on the GOULD unit, the subroutine also calculates and sends to the printer the three dimensional coordinates of each of the workspace boundaries in five degree angle increments from -180° from horizontal line of sight to +180°. The coordinates are given in the aircraft system of coordinates. The listing also gives the coordinate of the eye location in the aircraft system. Figure 16 shows the coordinate data for the plot in Figure 14.

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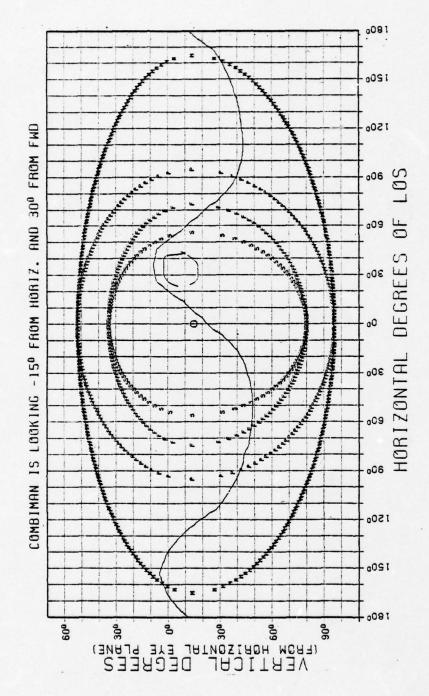


Figure 15. Sample Visibility Plot - Off Angle View.

CBHO4 --- COMBINAN PROGRAM, VERSION 4

VISIBILITY PLOT DATA FOR COCKPIT CANOPY CLEARLINE YE LOCATION IN AIRCRAFT SYSTEM (262.26, 0.0 ,133.58)

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	AIRCRAFT COORDINATES	-15.896	-16.795	-17.078	-11.209	-17.323	-17.510	-17.679	-17.816	-17.920	-17.99d	-18.214	-18.381	-18.472	-18.622	-18,882	-19.080	-19.300	-18.799	-16.294	-13.703	-11.000	-8.297	-5.541	-2.176	
	AIRCR FS	253.083	254.429	256.045	257.649	259.206	260. 129	262.261	263.819	265.420	267.083	268.890	270.832	212.925	275.300	278.104	281.341	285.261	289.109	290.483	291.646	292.483	293.224	293.688	293.986	
	HOR12	09	65	02	15	80	82	06	95	001	501	011	115	120	125	130	135	140	145	150	155	160	165	170	115	
0.0 ,133.581	NATES	115.660	117.404	119.302	121.453	124.144	126.100	127.876	129.475	131.248	133.007	134.514	134.758	135.000	134.758	134.514	133.007	131.248	129.475	127.876	126.100	124.144	121.453	119.302	117.404	
(262.26,	DORDI	15.891	14.729	13.540	12.323	11.036	9.620	8.244	6.852	5.477	4.100	2.731	1.362	0.0	-1.362	-2.731	-4.100	-5.477	-6.852	-8.244	-9.620	-11.036	-12.323	-13.540	-14.729	
I SYSTEM	AIRCRAFT C	253.086	251.547	250.899	249.938	249.109	248.522	241.982	241.567	247.212	246.559	246.775	246.692	277.911	246.692	246.175	246.959	247.212	247.567	247.982	248.522	249.109	249.938	250.899	151.941	
IN AIRCRAFT	HOR 12.		-55	-50	-45	-40	-35	-30	-25	-20	-15	01-	-5	•	s	01	15	50	52	30	35	0,	45	20	55	
EYE LOCATION I	TES HL	135.500	134.490	133.502	132.024	129.841	127.091	123.642	119.546	116.665	116.290	115.983	115.731	115.513	115.333	115.174	114.987	114.887	114.740	114.579	114.420	114.302	114.265	114.292	114.772	
	COORDINA	-0.000	2.111	5.541	8.297	11.000	13.703	16.294	18.799	19.300	19.080	18.882	18.622	18.472	18.381	18.783	17.998	17.913	11.787	17.647	17.510	17.323	17.178	47.063	16.195	
	AIRCRAFT C	294.470	294.004	293.688	293.224	292.483	291.646	290.483	589.109	285.261	281.341	278.104	275.300	272.925	210.832	269.097	267.083	265.419	263.817	262.261	260.129	259.206	257.658	256.050	254.429	
	HORIZ.		-175	-170	-165	-160	-155	-150	-145	-140	-135	-130	-125	-120	-115	-110	-105	-100	-95	-90	-85	-80	-15	-10	-65	

Figure 16. Sample Visibility Plot Printed Output for Cockpit Clearline Boundary in Figure 14.

SECTION 3

STRENGTH CAPABILITIES OF SEATED OPERATORS

The University of Dayton Research Institute supported a study to determine the capabilities of human subjects to exert forces on a triaxial force handle located within the subjects' reach. This study is being conducted by Dr. J. W. McDaniel of AMRL/HED. UDRI personnel performed modification, calibration, and maintenance of the HERCULES (Human Engineering Research to Cull Efficient Strength) apparatus located in AMRL/HED. UDRI personnel were also responsible for the collection of strength data from human subjects and the preliminary data analysis.

3.1 HERCULES LAB

The HERCULES apparatus and associated equipment has been made completely operational after a period of inactivity. Using a triaxial strain gauge transducer handle, this system can measure and record forces exerted by seated human subjects with 2% accuracy on forces up to 300 pounds in any direction. The handle was positioned in 76 locations relative to the SRP (Seat Reference Point) of the seated subject.

The equipment used for the data collection is shown in Figure 17 and consists of the triaxial force handle, a Honeywell Accudata 113 bridge amplifier system, a Honeywell 5600B 7-channel FM tape recorder, a Brush Mark 200 strip chart recorder, an audio amplifier and power supply, and a remote control unit.

3.1.1 Contractor-Built Equipment

3.1.1.1 Remote Control Unit

To simplify the experimenter's task, a remote control unit (shown in Figure 18) was designed and built to contain an exertion timer, dial encoder, strip chart ON/OFF switch, data switch, and tape

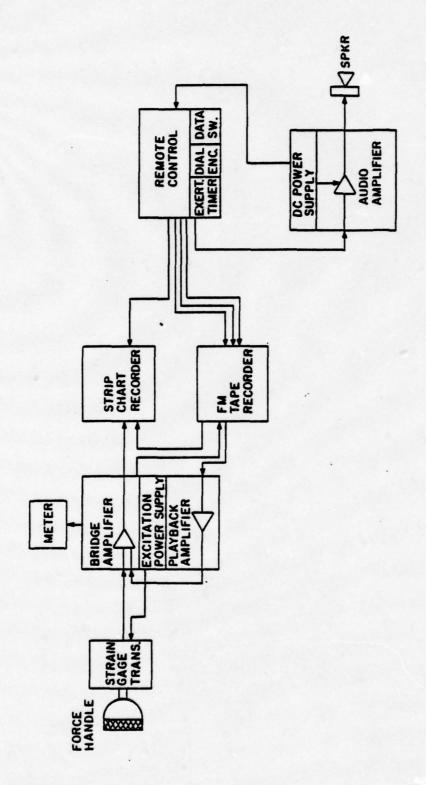


Figure 17. HERCULES System Component Diagram.

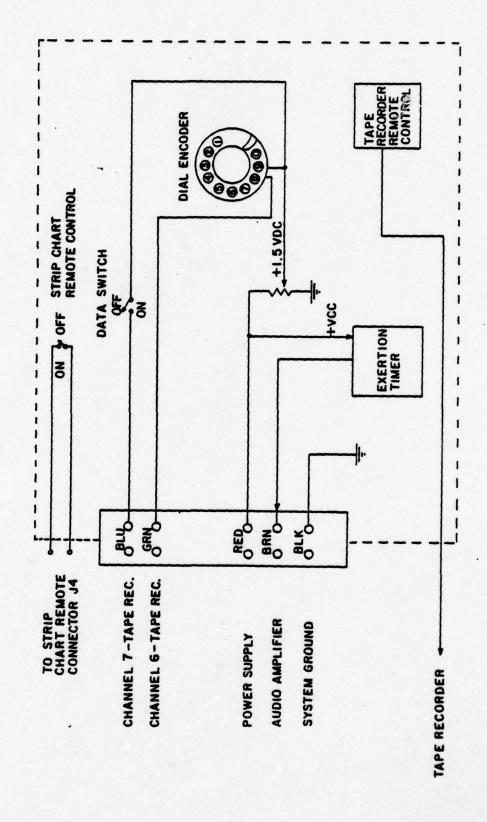


Figure 18. HERCULES System Remote Control Unit.

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recorder remote control. These functions were connected to the system with a ten-foot cable. The controls on the panel were arranged according to order and frequency of use. This arrangement places all frequently used functions at the experimenter's fingertips.

To provide an edit function, a data switch was installed on the remote control unit and was used to indicate valid (ON) or invalid (OFF) data on one channel of the tape recorder.

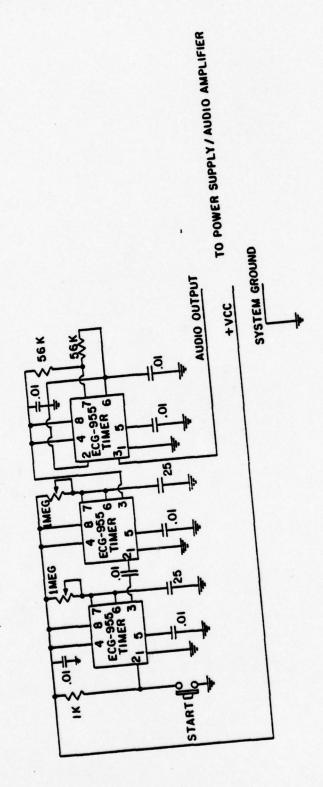
3.1.1.2 Timer Controlled Tone Generator

An electronic timer was designed and constructed to provide an auditory tone to cue the subject as to when to terminate the exertion. The timer consisted of three ECG-955 ICs (integrated circuits) performing three basic functions within the timer. The circuit diagram is shown in Figure 19.

IC1 was triggered by a pushbutton at the beginning of a force exertion and performed the main timing function of controlling the delay interval. This interval was adjustable from zero to two minutes but was normally set to five seconds. Triggered by IC1, IC2 controlled the duration of the auditory tone and was also variable from zero to 2 minutes in length, but was normally set to a $\frac{1}{2}$ second burst. IC3 was used as an audio oscillator and was turned on and off by IC2. The output of IC3 was connected to the input of the audio amplifier as shown in Figure 20.

3.1.1.3 Audio Amplifier

The audio amplifier was on LM380 IC capable of one watt audio output and was normally set well below this level. The audio output was coupled to a common speaker. The speaker was attached to the HERCULES handle mainframe assembly near the subject.



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Figure 19. Circuit Diagram for Electronic Timer.

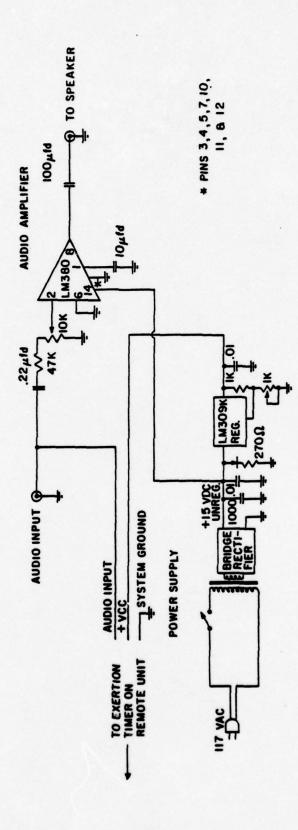


Figure 20. Diagram of the Power Supply and Audio Amplifier.

3.1.1.4 Power Supply

A power supply was built for the timer, audio amplifier, data switch, and dial encoder and is shown in Figure 20. Using an LM309K voltage regulator IC, the supply is adjustable from five to fifteen volts DC at up to 1 amp output current with internal overload protection.

3. 1. 2 Modifications to the Existing Equipment

3.1.2.1 Reference Resistors

The accuracy of the system has been improved through various modifications. Calibration efficiency required high-stability reference potentiometers as shown in Figure 21, to be installed and calibrated to simulate known forces in six directions. A weight stand was build to facilitate applying known forces on the handle. Its pulley system allowed a 100-pound force to be exerted on the handle in six orthogonal directions. A digital voltmeter was used to calibrate the reference potentiometers against the 100-pound weights.

3. 1. 2. 2 Noise Level Reduction

The system originally had a high noise level due to several unshielded connections. When these were corrected, the noise was reduced significantly.

3.1.2.3 Dial Encoder

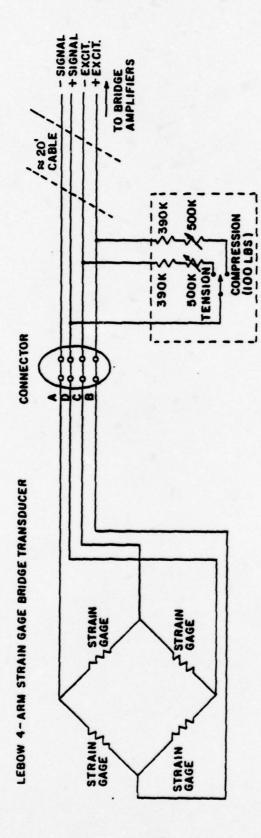
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A telephone-type dial encoder was used to generate pulses to identify calibrations, subjects, and handle positions during data collection. This was installed on the remote control unit.

3.1.2.4 Tape Recorder Remote Control

This unit was installed on the remote control unit.

However, there were no further modifications to it.



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Diagram Representing a Single Channel of a 3-Channel HERCULES Bridge Transducer System. Figure 21.

3.1.2.5 Remote Strip Chart ON/OFF Switch

A toggle switch was installed on the remote control unit to provide for remotely activating the strip chart paper drive mechanism.

3.2 PROCEDURES

Data collection procedures required modifications for two reasons: the equipment modifications, and analog data processing constraints. Because of constraints of equipment capabilities of the ASD Computer Center Hybrid Simulation Division, data collection procedures were modified to facilitate the conversion of analog data.

Through the process of identifying sources of errors in the data analysis system, several procedural improvements to the analog-to-digital conversion process were recommended. Additionally, a computer program was prepared to provide a means of organizing the data collection procedure and to provide an automated check of the digital data.

3.2.1 Computer-Generated Data Collection Format

A program named RANDM has been developed for the HERCULES experiment to print an experimental data collection sequence which contains information the experimenter needs to position the force handle, select a direction of exertion, and select a subject to perform that exertion. The programmer uses the IBM System Subroutine RANDU to generate the random numbers which, in turn, are used to generate the sequence of steps to be followed in the procedure. A detailed description of the subroutine RANDU can be found in the IBM Scientific Subroutine Manual (Reference 7). All random numbers generated by RANDU are 15 digit decimal numbers between 0. and 1.

3.2.1.1 Method

In order to assure a unique set of random numbers throughout each execution of the program RANDM a new 15 digit seed number is supplied to the random number generator the first time it is called by

RANDM. A random handle position number is found by multiplying the first random number obtained from RANDU by a number which is one greater than the number of positions possible, and truncating the result to an integer value. All exertion directions are then randomized for each subject within each position using the same randomization process. If the number of simultaneous subjects is n, subject i will start as the first subject of the first position, and subject i+1 will start as the first subject of the next position. This sequence is continued until the nth subject is reached. At this point the same sequence is repeated until all handle positions have been used. The last exertion is a sequence for a given handle position is a repetition of the first exertion direction/subject combination. For this repeated exertion, a constant (100) is added to the subject number to set it apart from the other subject numbers. This repetition is performed to provide a verification of the subject's performance reliability (see Figure 22). At the end of the program, the seed number to be used when the program is run again is printed out. This is done to make sure all numbers are randomized properly (see Figure 23). A flowchart of program RANDM is shown in Figure 24.

3.2.1.2 Program Input Data

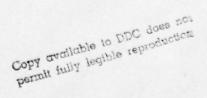
The first data card read by the program RANDM gives information on the number of exertion directions (nexr), handle positions (npos) and simultaneous subjects (nsub) which are to follow. Any number up to 9 exertion directions, 99 handle positions, and 5 simultaneous subjects are possible. These numbers are right justified (see Figure 25a).

The following group of <u>nexr</u> cards will be the exertion directions. Each card contains one exertion direction number (<u>iexr</u>) and its 8 character name (<u>exertion-direction name</u>). The exertion direction number is an integer and is right justified in the field (see Figure 25b).

The second group of <u>npos</u> cards read will each have one handle position number (<u>ipos</u>) and the three dimensional coordinates of that handle position (<u>lat dim</u>, <u>fwd dim</u>, <u>vert dim</u>), as shown in Figure 25c.

	SUBJECT NO.	NAME	EXERTION	DIRECTION
1	7301	PAT	404	CCAN
2	7302	TOM	204	RIGHT
3	7301	PAT	504	FCR EWARD
4	7302	TOM .	304	UP
5	7301	PAT	104	LEF T
ó	7302	TOM	504	FCREMARD
7	7301	PAT	304	UP
8	7302	TCM	604	EACKWARD
9	7301 .	PAT	204	RIGHT
10	7302	TCM	104	LEFT
11	7301	PAT	604	BACKWARD
12	7302	TOM	404	DCMN
13	7431	PAT	404	CCAN

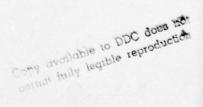
Figure 22. Sample Data Collection Sequence, with Subject 1 Repeated.



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	SUBJECT NO.	NAME	EXERTION	CIRECTION
144	7302	TOM	507	FCREWARD
145	7301	PAT	oC7	EACKWARD
146	7302	TOM	207	RIGHT
147	7301	PAT	567	FCREWARD
148	7302	TOM	607	EACKWARD
149	7301	PAT	207	RIGHT "
150	7302	TOM	367	LP
151	7301	PAT	167	LEFT
152	7302	TOM	107	CEFT
153	7301	PAT	407	CCWA
154	7302	TGM	407	CCMN
155	7301	PAT	307	LP .
15ò	7402	TOM	507	FCREWARD
	NEA SEED TO	BE USED =	727020575.	

Figure 23. Sample Data Collection Sequence, with New Seed Number Printed.



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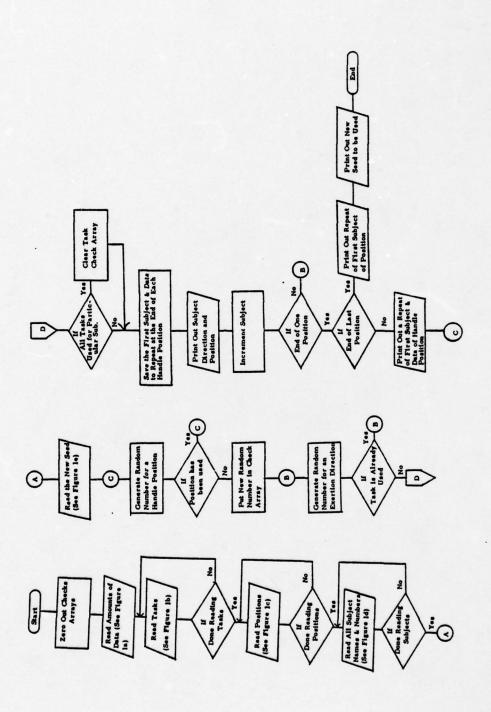


Figure 24. Flow Diagram for Program RANDM.

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	TX9i 0-	/////		exertion direction name 99999	tion tion	00 00 00 00 00 00 00 00 00 00 00 00 00	6 2	6.5	9 2 2 3	000	en ≘	5 2	50 €	on %	3.00	& & & & & & & & & & & & & & & & & & &	9 9 9	9 8	6 6	67 3	(a) (b) 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	6 6 8	07	Q	9 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	00 3	Q 1	en 2 en 3	& 3 & 4	9 3	6 3	93	. es s	9.2	60 22	60 3	6 6 6	03	8 9 9	00	on 83	9 5	# # # # # # # # # # # # # # # # # # #	92	9 %	95	98		
49	////जिन	71111111111	soqi es a	mib .tsl a		mib .bwl es	66:	mib Jreve 2	9.5	6.5	6.5	60 %	65%	5 5 5	9 2	6 8	9 8 8 8	6 8	0 5	6 6 8	(c)	1 - 9	6 A 6	9.8	60 7	603	9 3	9.3	0.3	9 8 8 9 2 2 2 2 2 2 3 4 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5	6 3	63	9 8	90 90	6. 8. 6. 8.	9.3	9 9	0.3	0.3	9 6 6	5.3	9.5	002	9 2 2	9 5	9 9	68		
Conv	6-	65 %	qnst o	1/1/1/5/5	o-	6.5	6 2	62	9 9 9 1 1 1 1 1 1	6 9	6 2	6 8	6 2	662	30.	6.8	60 %	60 g	9 5	9 20	(d) (e) 9 9 9 9 9 9 9 9 9	0 8	9.00	9. 8. 9. 8.	6 6	6 3	9 9 9 8 9 9	60 F	9 4	9.2	. 50%	60 3	9 3	93	e 8	6.3	003	es 3	e 2 e 2 e 3	5 5	60 3	9.5	on 2	9 2	9 2 9	00 0	9 2	0.8	
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	o-	9.0	6.5	6.9	o-	6.6	9 9 9 9 9 9 9 11 11 12 13 14 15 1	9 9 9	9 5	6.3	60 E	5,5	Fig. 999	Figure 9 9 9 9 9 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 6 2	25.	. 57 %	. In	9 6 6 E E E	ut I 299	Input Data 99999 2011 20 11 20 20 20 20 20 20 20 20 20 20 20 20 20		9 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	19 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	9 9 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	8 f	mats for 99999999999999999999999	Formats for Program RANDM. 999999999999999999999	9 9 9	ra 9 8	8 60 8	8 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	9 9 9 8 8 8 8 8 8 8 8 8	OM.	. 60 22 82 90 22	9 9 9	9 3	9999	cn :2	6.3	6.3	5 2	6 2 2	9 2 2	9 2 2	92	# # # # # # # # # # # # # # # # # # #	on 2	

The third group of <u>nsub</u> cards read will each contain one subject number (<u>isub</u>) and the subject's first name (<u>subject name</u>). The subject number is an integer value and should be right justified (see Figure 25 d).

The last card read should be the initial seed number for the program. The seed is right justified and must have a decimal point at the right-most position (see Figure 25e).

3.2.1.3 Program Output

The first output format generated is a repeat of the input data. This provides a means of verifying the input data (see Figure 26).

The second output format contains random position number, its three-dimensional coordinates, and its associated experimental data collection sequence. This consists of all exertion directions, randomized for each subject. This format will be used for all handle positions. No handle positions are repeated, and for each position no exertion directions are repeated for any one subject.

In addition to printing the output on paper this program will also punch the output data on cards for use in verifying the experimentally gathered digital data.

INPUT 0 12 1 LEFT 2 RIGHT 3 UP 4 DOWN 5 FCREWARD 6 BACKWARD 1-20 20 40 2-20 10 40 3-20 0 40 4-20 3C 30 5-20 20 30 6-20 10 30 7-20 30 20 8-20 20 20 9-20 10 20 10-20 30 10 11-20 20 10 12-20 10 10 7301 PAT 7302 TCM 1397643.

Figure 26. Repeat of Input to Program RANDM.

SECTION 4

MULTIPLE BIVARIATE PLOTTING PROGRAM (BIVPLOT)

A considerable effort was made during this contract period to develop a plotting program (BIVPLOT) to plot the frequencies of two anthropometric variables which the user has selected from two surveys. The frequency data from the two surveys are plotted within the same table. Built into BIVPLOT is the capability of producing single survey tables as well. Both of these can be used with data in either English or metric units. Only the general layout and statistical computations could be used from the existing AMRL bivariate program which was made to produce single surveys on a computer line printer. An example of the output of this program is shown in Figure 27. While attempting to adapt this program for multi-survey plots on the printer it was found that the maximum number of print-characters contained in one printline was not large enough to accommodate the number required by the multisurvey plots. Because of this, it was necessary to write the program for a computer plotter, rather than printer. The change from single to multiple survey tables necessitated a new input routine be established to handle the data from two surveys simultaneously.

4.1 THE PLOT

Subroutine TABLE was then written to produce a suitable table outline in which to plot the frequencies for the surveys' selected variables. Written for a general case, it produces only as many rows and columns for frequencies as are needed for each individual table. Control is returned to program BIVPLOT where the frequencies are then plotted and summary statistics for each survey can be calculated and plotted with each table. An example of this output is shown in Figure 28.

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62												-						-				
28								-										-		15	. 5	30
27							-											-			1677.5	30
92																						62
52					-	~		-										•			1657	1957
23 24 25	-								-		-							m		13	• •	92
23									2		-		-					3			1637	1937
22					-	-	~		-		-	-						-		12	• •	22
21																					1617	1917
20				-		-			~	-		-						9		==	5.2	55
13									2	~	-	-						9			159	1.89
18				-				-		-	-	-	-	-				2		10	5.2	25
11																					157	187
16												~	~	m				1		6	5.2	24
15										-	m	-	S	~	-			13			155	185
;											-	~	-	3	~	~		12		•	2.2	23
13											-	~	3	N	m	m	-	16			153	143
12																				-	5.2	22
7														N	9	~	-	11			151	-
70												-	~		*	3	-	12		9	5.1	21
•														-	m	S	m	12			149	170
7 8 9 10 11 12 13 14 15 16 17 18 19														-	•		~	9		5	17.5	20 21 22 23 24 25 26 27 20 29 1777.6 1777.6 1777.5 1897.5 1917.5 1937.5 1957.5
-																					1,4	
•									*					~	~	*	~	2		*	51.5	19
4																2	~	3			1457	1,
*																			UMNS	3	1437.5	18
~																			FOR COLUMNS	~		17
-														-		-		~			1417.5	1717
	257.50	247.50	237.50	227.50	217.50	207.50	197.50	187.50	177.50	167.50	157.50	147.50	137.50	127.50	117.50	107.50	97.50	TOTAL	41DVALUES	-	1397.5	1697.5

R REGRESSION EQUATIONS & STD ERROR 1297.736 71.93 .776 = (2.747)* MEIGHT -231.347 71.93 .770 = (.220)* HEIGHT 1677-25 114-46 138-16 32-42 ASSORTED STATISTICS
HEIGHT
MEIGHT Figure 27. Line Printer Output for a Single Survey from Program BARE BIVAR.

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A BIVARIATE FREQUENCY TABLE FOR SITTING HEIGHT AND STATURE USAF MEN/USAF WOHEN

	67.7	03.7	02.7	01.7	6.9	2.3	6.3	11.7	6.3	-	7	5	2.3	91.7	6.9	100	6.3	11.1	100	6.3	11.7	13.7	12.7	11.3	0.0	19.1	78.7	7.1	78.2	2.3	TOTAL	USAF H	S	S	SAF H	S	•
	1			-	-	-	-	-	-	-	-	-	1	-	-	-	-	-	-	-		/	1	1	-	/ 8 /	7	+	1		5	HEN	=	SITTING HEIGHT	USAF WOMEN ASSORTED	STATURE(CM)	THUIS OF TAIL
	1	-		-	-	-	L	-	-	1	-	-	-	-	-	-	-	-	-	-		-	-	-	1	1	7	1	-	-	/	ASSORTEG	ECCH	0 14	ASSO	ECCH	
1	4	-				_		-	L	-	-	-	-	-	-			-	-		1	1	1	1	7	-	7	7	-	1	1	RTEG	_	THOI	RTED	-	
-	+	-		-	-	-	-	H	-	-	-	-	-	-	-	-	-	_	-	1	8	*	7	18	1 81	-	1	*	1	-	15			3	-		
1	+	-			-		-	-	-	1	-	-	-	-	-	-	-	F		1	01,	114	=	2	=	9	•	•	1	-	4	STATISTICS			STATISTICS		
31,5	+	-		-	-	-	-	-	+	+	-	-	-	-	-	-	-	=	*	8 /	13/	118	38	•	95	10	8	-	+	-	1	TICS			TICS		
1	1	-		-	-		-	-	-	-	-	-	-	-	-	-	- /	-	111/	91/	137	(13	/38	120	187	-	+	3	+	-	7						
	1	1						-	-	-		-	-	-	-		8 /	118	188/	118/	987	7 48	(3)	(13	9		1	+	+	1	7	MEAN	177.34	93.18	NEAN	162.10	-
:	1	1				-		-	-	-	-	-	-	F	-		118	/ 30	144	61/	140	11,	827	712	-	=	+	+	1	-	7	Z	34	19	z	2	-
	+	1					-	-	-	-	F	-	8 /	-	• /	1	/83	/3416	/48	1 88/	144	118	•		7		+	1	+	1	73	ST DEV	8.1	3.18	ST DEV	6.00	
1	1	1				-	-	-	-	-	1	-	-		1 71		183/	1/33/1	/ 36	00/	98/		7	-	1		1	1	1		73				EV	0	1
1	1	1					-	-	-	-	1		1	10 /1	1/102	1 22 /	118/1	101/2	1/34	03/1	1/10	3 /1	7	1	1		H	1	1		1	~	0.788	0.708	~	0.801	-
1	1	1				-		-	-	-	F	1	100	10/1039	131/	5/36/8	133/6	101/6	9/16	01/1	k /	6 /			-			1	1		<u> </u>						
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DATE: 11/16/76
HETRIC
PLOT: 48

Figure 28. Metric BIVPLOT Output.

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4.2 TABLE OF CONTENTS

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Each bivariate table is also dated, numbered, and labeled as containing either METRIC or ENGLISH data. The numbering is done to keep track of the large volume of plots which are anticipated. Program CONTENTS was written to keep track of these plots. It uses the variable number of the sets of user-selected anthropometric variables with their respective plot numbers to produce a cross-reference table of contents for the plots. A sample cross-reference table is shown in Figure 29.

4.3 BIVPLOT MULTIPLE SURVEY TAPES

Data surveys used in generating bivariate tables are stored primarily on individual magentic tapes. Handling two complete data survey tapes simultaneously, to generate a set of plots takes a considerable amount of computer time. The two surveys of interest have been the 1967 USAF MEN and the 1968 USAF WOMEN surveys. The primary interest in these surveys has been to see the relationship between sizes of men and women, to assist in the process of sizing uniforms and equipment to fit both males and females. To reduce input time for the plots using these surveys, 72 variables, which were common to both surveys were selected from the 204 variables in the men's survey and the 156 variables in the women's survey. These 72 selected variables were judged to be most useful for the sizing procedures. The common variables from the two survey tapes were combined into one tape containing all the pertinent information needed to run any combination of these variables over both surveys. In combining the tapes, all data were converted to metric units (cm/kg/years). The pertinent information for each variable included new range data based on the overall minimum and maximum values over both surveys, a plot step size factor, and a conversion factor for converting the metric unit to an English unit. Figure 30 shows the comparable variables from both surveys, and gives the range of values for each variable in the original unit of measurement. Figure 31 shows the data contained on the combined tape.

BIVARIATES FOR USAF MEN VS. MONEN (METRIC/ENOLISH PLOT NO.)

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Table of Contents for 1967 USAF Men Vs. 1968 USAF Women Plots; Plotted by Program Contents. Figure 29.

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Page 2 of 4

Figure 29 (Continued)

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14 EYE MEIOHT-SITTING
16 NIGHOULDER MEIOHT-SIT
16 ELSON REST MEIOHT-SIT
17 POPLITER, MEIOHT-SITING

12 LATERAL MALLEGLUS HETOHT

IN SITTING HEIGHT

6 BUFRASTERNALE MEIGHT
7 TROCHANTERION MEIGHT
8 BUTTOCH MEIGHT
9 OLUTEAL FURRON MEIGHT
10 CROTCH MEIGHT

4 CERVICALE HEIGHT

Figure 29 (Continued)

Page 3 of 4

19 BUTTOCK-KHEE LENOTH
20 RCROHION-RROINE LENOTH
21 RADIRLE-STYLION LENOTH
22 SHOULDER CIRCUMFRENCE

29 CHEST CIRC AT SCYE

IS BUTTOCK-POPLITER LENOTH

31 VERTICAL TRUM CIRC

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Figure 29 (Continued)

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NO.	SURVEY		MUMINIM	MUMIXAM	SURVEY		MINIMUM	MUMIXAM
1	1	AGE	2100.00	5050.00	1	AGE	177.50	505.00
2	2	WEIGHT	117.50	264.00	2	ME IGHT	82.50	200.00
3	13	HEIGHT (STATURE)	1577.50	1972.00	7	STATURE	1442.50	1830.30
4	14	CERVICALE HEIGHT	1342.50	1702.00	9	CERVICALE FEIGHT	1202.50	1500.00
5	15	ACROMION HEIGHT	1277.50	1644.60	10	ACROMIAL HEIGHT	1142.50	1520.CO
6	19	SUPRASTERNALE HGHT	1267.50	1623.00	11	SUPRASTERNALE HUHT	1102.50	1500.00
7	24	TROCHANTER ION HIGHT	787.50	1119.00	15	TRECHANTER IC HEHT	682.50	965.00
4	23	BUTTOCK HEIGHT	767.50	1098.00	16	BUTTOCK HE IGHT	044.50	900.00
9	25	GLUTEAL FURROW HGT	642.50	586.00	17	GLUTEAL FURROW HGT	582.50	864.00
10	26	CROTCH HEIGHT	712.50	1035.00	19	CROTCH HEIGHT	002.50	875.00
11	31	ANKLE HEIGHT	103.50	183.00	20	ANKLE FEIGHT	72.50	160.00
12	132	LAT L MALLEDLUS HT	53.50	89.00	21	LAT L MALLEOLUS HT	47.50	87.00
13	32	SITTING HEIGHT	ac7.50	1048.00	23	SITTING HE IGHT	752.50	964.30
15	33	MIDSHOULDER HT/SIT	537.50	746.00	24	MIDSHOULDER HT, SIT	632.50	831.00
16	36	ELBON REST HGT/SIT	152.50	351.00	25 27	EL BOW REST HEIGHT	502.50 142.50	295.00
17	38	POPLITEAL HGHT/SIT	362.50	512.00	28	POPLITEAL HEIGHT	332.50	471.00
18	40.	BUTTOCK-POPLITEAL	422.50	598.00	29	BUTTOCK-POPLIT L L	382.50	585.00
19	39	BUTTOCK-KNEE LNGTH	517.50	650.00	30	BUTTOCK-KNEE LNGTH	482.50	664-00
20	43	ACROMION-RADIALE L	271.50	393.00	31	ACROMION-RADIALE L	252.50	365.00
21	45	RADIALE-STYLION LH	224.50	314.00	32	RACIALE-STYLION L	187.50	280.00
22	67	SHOULDER CIRCUM CE	997.50	1367.00	37	SHOULDER CIRCUMFER	862.50	1221.00
23	68	CHEST CIRC AT SCYE	792.50	1243-00	38	CHEST CIRC AT SCYE	702.50	1035.00
24	9	CHEST CIRCUMF ENCE	772.50	1214-00	39	BUST CIRCUMFERENCE	742.50	1139.00
25	70	WAIST CIR-OMPHAL N	677.50	1246-00	41	WAIST CIRCUMPERNCE	522.50	951.00
26	72	BUTTOCK CIRCUMF CE	812.50	1244.00	44	HIP C-9 BLW WAIST	762.50	1201.00
27	96	UPPER THIGH CIRCUM	452.50	759.00	45	UPPER THIGH CIRCUM	422.50	720.00
28	98	KNEE CIRCUMPERENCE	312.50	482.00	46	KNEE CIRCUMPERENCE	302.50	457.00
29	100	CALF CIRCUMF/RIGHT	297.50	452.00	47	CALF CIRCUM, RIGHT	262.50	445.00
30	102	ANKLE CIRCUMF ENCE	181.50	267.00	49	ANKLE CIRCUMPERNIE	172.50	256.00
31	74	VERTICAL TRUNK CIR	1422.50	1975-00	50	VERTICAL TRUNK CIR	1342.50	1782.00
32	75	VERT TRUNK CIR/SIT	1367.50	1856.00	51	VERTICAL TRK C.SIT	1322.50	1705.00
33	73	SCYE CIRCUMFERENCE	867.50 402.50	594.20	52 53	SCYE CIRCUMFERENCE	842.50	1284-00
35	103	BICEPS C-EXTENDIRT	227.50	388.00	55	BICEPS C.RELAXED,R	282.50 192.50	374.00
30	106	BICEPS C-FLEXED/RT	252.50	408.00	56	BICEPS C.FLEXED, R	192.50	390.00
37	109	ELBOW CIRC-FLEXED	258.50	369.00	59	ELBOW CIRC, FLEXED	212.50	358.00
38	111	LOWER ARM C-FLEXED	241.50	354.00	61	FOREARM C. FLEXED	192.50	328.00
39	112	WRIST CIRCUMF ENCE	150.50	268-00	62	ARIST CIRCUMFERNCE	122.50	176.00
40	50	BIACHOMIAL BREADTH	337.50	474.00	63	BI ACROMIAL BREADTH	307.50	410.00
41	. 51	BIDELTOID BREADTH	397.50	567.00	64	BIDELTOID BREADTH	342.50	501.00
42	52	CHEST BREADTH	257.50	415.00	65	CHEST BREADTH	222.50	359.00
43	55	HIP BREADTH	282.50	446.00	68	HIP BREADTH	282.50	441.00
44	64	BUTTOCK DEPTH	170.50	338-00	77	BUTTOCK DEPTH	152.50	306.00
45	65	THIGH CLEARANCE HT	124-50	217-00	78	THIGH CLEARANCE	87.50	169.00
40	118	SHOULD ER LENGTH	131.50	217.00	79	SHOULDER LENGTH	112.50	188.00
47	120	INTERSCYE	270.50 492.50	514.80	82	INTERSCYE	272.50	442.00
48	124	INTERSCYE MAXIMUM HAIST BACK-OMPHL N	402.50	713-00 563-00	83 85	INTERSCYE, MAXIMUM WAIST BACK	372.50	481.00
50	49	SLEEVE INSEAM	397.50	578.00	87	SLEEVE INSEAM	362.50	535.00
51	115	SLVE L/SPINE-WRIST	787.50	1045.00	90	SPINE-TO-WRIST LIH	672.50	912.00
52	134	HAND LENGTH	166.50	222.00	91	HAND LENGTH	152.50	220.00
53	136	HAND BRIMETACARPLE	75.50	102.00	92	HAND BREADTH	60.50	88.00
54	130	HAND C/METACARPALE	143.50	247.00	93	HAND CIRCUMFERENCE	147.50	215.00
55	125	FOOT LENGTH	231.50	313.00	94	FOOT LENGTH	207-50	270.00
50	127	FOOT BREADTH	83.50	117.00	95	FOOT BREADTH	67.50	110.00
57	150	HEAD LENGTH	174.50	226.00	96	HEAD LENGTH	162.50	207.00
58	156	HEAD BREADTH	138.50	176.00	97	HEAD BREADTH	122.50	171.00
59	141	HEAD CIRCUMFERENCE	526.50	620-00	98	HEAD CIRCUMFERENCE	497.50	617.30
60	144	BITRAGION-CORONAL	320-50	402.00	112	BITRAGICN-CORONAL	287.50	392.00
61	162	BIOCULAR BREADTH BITRAGION BREADTH	77.50 123.50	108.00	113	BIOCULAR BREADTH	78.50	112.00
63	158	BIZYGOMATIC OR DTH	123.50	159.00	115	BITRAGION BREADTH	112.50	152.00
64	160	BIGONIAL BREADTH	94.50	142.00	116		108.50	149.00
05	165	NOSE BREADTH	24.50	51.00		NASAL BREADTH	22.50	122.00
00	166	LIP LENGTH	38.50	66.00		LIP LENGTH	30.50	58.00
67	171	MENTON-SUBNASALE L	52.50	89.00		MENTON-SUBNASALE L	38.50	75.00
68	172	MENTON-NASAL ROOT	97.50	143.00		MENTON-SELLION LTH	86.50	128.00
69	168		38.50	64.00		SUBNASALE-SELLIUN	30.50	61.00
70	154	EAR LENGTH	48.50	83.00	123	EAR LENGTH	34.50	09.00
71	153	EAR BREADTH	24.50	51.00	124	EAR BREADTH	18.50	42.00
72	12	GRIP STRENGTH	32.50	86-00	1.25	GR IP STRENGTH	9.50	53.00

Figure 30. Survey Variable Names, Numbers and Ranges from the Individual Survey Tapes.

	CAAD					
14,1954.1,/,(2054.1))						
	~	10.50	27.00	1.50	1.0000000	_
	و	37.42	119.75	3.00		S
		144.25	197.20	2.00	_	CAD CEND
-	10 1	120.25	170.20	2.00	_	
		114.25	164.40	2.00		
	-	116.25	162.30	7.00		
HEIGHT		68.25	111.90	1.50		
		64.25	109.60	2.00	0.3937008	
N HEIGHT	21	54.25	99.66	1.50	0.3937008	(CH) (IN)
_	13	60.25	103.50	1.50		(CH) (IN)
	12	1.25	16.30	0 * * 0	•	CH) (H)
LUS HEIGHT	54	4.75	06.8	0.20		(CH) (IN)
		75.25	104.80	1.00	0.3937008	(CH) (IN)
		63.25	91.00	1.00	0.3937008	(CH) (HO)
_		50.25	14.60	1.00		
	21	14.25	35.10	0.40		(CH) (IN)
	54	33.25	51.20	0.60	0.3937008	(CH) (IN)
ENGTH	54	38.25	29.80	0.90		(CH) (EN)
BUTTOCK-KNEE LENGTH	61	48.25	9.69	0.0	0.3937008	(CH) (IN)
I	23	25.25	39.30	0.60		(CH) (IN)
	22	19.75	31.40	09.0		(CH) (IN)
ENCE	22	86.25	136.70	2.00	0.3937008	(CH) (IN)
	91	70.25	124.30	2.00	0.3937008	(CH) (IN)
	19	14.25	121.40	2.00		(CH) (IN)
	20	52.25	154.60	2.50		(CH) (IN)
RENCE		76.25	124.40	2.00		CHI (IN)
	16	45.25	15.90	1.50		
	91	30.25	48.20	09.0	•	
RIGHT	54	25.25	45.20	08.0		
		17.25	26.70	24.0		(CH) (IN)
	-	34.25	197.50	2.50	_	CH) (IN)
IRC, SIT		132.25	185.00	2.00		(CM) (IN)
	16	84.25	141.10	2.00		CM) (IN)
	19	29.25	29.40	1.50		CH) (IN)
	23	19.52	38.80	0.80		(CH) (IN)
DIRIGHT	54	19.25	40.80	0.80		(CH) (IN)
	17	21.25	36.90	0.60		(CH) (EN)
E0	21	19.25	35.40	09.0	0.3937008	(CM) (IN)
	19	12.25	20.80	0.40		(CM) (EN)
BIACROHIAL BREADTH	18	30.75	47.40	0.60	00.3937008	(CM) (IN)
ADTH	17	34.25	50.70	0.80	0.3937008	(CH) (HO)
CHEST BREADTH	13	22.25	41.50	0.80	0.3937608	(CM) (EN)
	11	28.25	79.44	9.0	0.3937000	(CH) (EN)
	13	15.25	33.86	0.8	0.3937008	(CH) (IN)
THIGH CLEARANCE HEIGHT	22	75	21 30		0000000000	TOWN CTAIN
	,		00.17	9.0	000756600	101111111

Figure 31. Combined Tape for Input to BIVPLOT.

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311 192

300 161

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531 324 159

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0.3937008

In a like manner, the Health Examination Survey of men and women were put on another tape for their analyses.

4.4 EQUALIZING SAMPLE SIZES

In order to make these multiple bivariate plots (multi-bivplots) as useful as possible, the sample sizes were equalized. It was decided that only the first 2000 subjects from the 1967 USAF Male survey would be used, and datasets for 95 subjects would be added to the 1905 subjects on the 1968 USAF Female survey. These 95 datasets were chosen at random using a UDRI-written program, RANDOM, which, in turn, employed a random number generating routine from the CDC 6600 computer system. The original 2420-subject data values from the 1967 survey and the 1905-subject data values from the 1968 survey were used to caluclate the summary statistics.

4.5 SUMMARY

To date one English and 162 metric plots have been generated from the 1967 versus 1968 USAF surveys tape. Each plot is approximately 14"x10" in size and is plotted using a .2 mm India ink pen on the offline CALCOMP plotter at the ASD Computer Center (Building 676). Plot tapes are generated on the CDC 6600 computer system at Building 676 using the CDC 1700 remote job entry terminal at Building 441. These plot tapes are then read by the CALCOMP 780 magnetic tape unit and plotted with a CALCOMP 763 digital incremental zip-mode plotter. This route has offered the best resolution and quality of output. However, because of the time required to generate these plots on the CALCOMP plotter, only ten plots can be produced a day. Once the plots have been produced, they are reduced to $8\frac{1}{2}$ x11 inch size on a reducing copy machine in Building 676 for their general use.

The original and primary use for these plots by AMRL has been for the recent series of chemical warfare clothing and personal equipment sizing and fit tests. These multi-bivplots have been an aid in sizing face respirators, protective garments, and gloves for both men and women in the ground forces.

Further multi-bivplots are expected to be produced and used in the future. Program BIVPLOT, however, is not fully documented and further changes are to be made to BIVPLOT during the next contract period. A series of these bivariate plots will be published in 1977 along with a more extensive documentation of program BIVPLOT and its accompanying subroutines. At that time the input formats for BIVPLOT will also be documented in full.

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SECTION 5 BIOSTEREOMETRIC DATA

This section contains the analysis of a new set of data obtained during this contract period. This set of data was collected for AMRL/HED by R. E. Herron et al., of the Biostereometrics Laboratory at the Texas Institute for Rehabilitation and Research, for the purpose of collecting mass distribution measurements for six anatomical specimens using biostereometrics (see Reference 8). This was done in conjunction with Chandler et al. (see Refer-9) who used the pendelum method to gather mass distribution data on these same specimens.

5.1 HERRON'S BIOSTEREOMETRIC DATA

Herron's biostereometric cadaver data were obtained from AMRL during the contract period covered in this report, and some preliminary statistical analyses were performed on the data using program HER1. The substance of Herron's data was published in AMRL-TR-75-18 pages 56-193 (Reference 8).

Statistical analyses performed on these data have been the following:

- A. New densities, called DENSITY 4, were calculated using Herron's volumes and measured cadaver weights, as reported in the Department of Transportation (DOT) report DOT HS-801 430, for each segment.
- B. A mean DENSITY 4 was calculated for each segment.
- C. Segment weights were recalculated using the DENSITY 4 mean value and Herron's volumes.

5.2 INPUT

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Input for HER1 consisted of: a numbered variable name card for each segment, using a format of (I4, 1X, 3A4); a card for each segment with the DOT reported densities and weights for each of the six cadavers, using format

(I2, 2X, 6(F6.4, F6.1)); tables 9, 21, 33, 45, 57, and 69 from Herron's data, each followed by a blank card. Format information for Herron's data is shown in Figure 32.

5.3 SUMMARY

Figure 33 shows the general flow of program HER1, which was used to perform the original data analyses. Figures 34, 35, and 36 show the DOT input, the first two tables of the Herron input, and the output for the first three cadaver segments respectively.

No further analyses of the biostereometric data has been planned, pending discussions with Dr. Herron at the Biostereometrics laboratory regarding his data.

Each punched card corresponds to one line of the data in the tables. The first two numbers of the cards represent the table number and the data line of that table, respectively. The numbers that follow are the same as those of the data in the tables. (Disregard the last 8 digits of each pink card.)

For example a card with: 34 19 3 1206388.6 1491387.0 3717724.4

is from the 34th table, the 19th data line (column headings, titles, and subtitles were not numbered) and the next 4 fields are the data.

Twelve different formats were used for the cards:

Format #	Table #
1	Table 1, lines 1-16
2	Table 1, lines 17-22
3	Tables 2-7, odd lines
. 4	Tables 2-7, even lines
5	Table 8
6	Tables 9,13,17,21,25,29,33,37,41,45,49,53,57,61,65,69,73,77
7	Tables 10-80, except those listed above
8 .	Tables 81-116, lines 1,4,7,10,13,16,19,22,25
9	Tables 81-116, all other lines
10	Tables 117,119,121
11	Tables 118,120,122
12	All table titles, subtitles, column headings

The Fortran coding for the above formats is as follows:

STATE OF THE PARTY OF THE PARTY

Format	(1)	13,16,3X,12,F27.3,2F16.3
Format	(2)	13,16,3X,12,F27.3,F16.3,F6.3,F10.3,F6.3
Format	.(3)	I3,I6,3X,I2,F10.1,F12.2,F13.1,F10.1,F12.1
Format	(4)	13,16,25X,F15.1,F10.1,F12.1
Format	(5)	I3,I6,3X,I2,F17.1,F6.1,F7.1,F13.1,F6.1,F7.1
Format	(6)	I3,I6,3X,I2,F10.3,F10.1,F9.2,F11.1,F8.1,F9.1
Format	(7)	13,16,3X,12,F17.1,F20.1,F20.1
Format	(8)	I3,I6,3X,I2,F17.10,2F20.10
Format	(9)	I3,I6,SX,F17.10,2F20.10
Format	(10)	I3,I6,3X,I2,F14.1,F17.1,F16.1,F14.1
Format	(11)	I3,I6,3X,I2,F12.2,F14.2,F16.2,F15.2
Format	(12)	20A4

Figure 32. Format Information for Herron's Data (Reference 8).

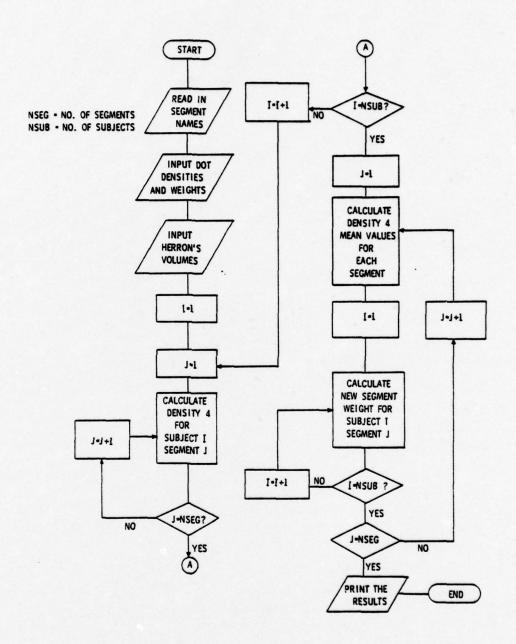


Figure 33. General Flow of Program HER1.

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	1094	سلنلا	usu	1173	1337	1410	1029	419	LCEL	427	LUQZ	_14
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11	1035	5639	1313	8082	1520	9399	1317	2000	1001	6090	1030	573
-12	1497	2246	1149	3039	1002	3794	1074	ے دیاعہ	1641	_25.64_	1358	_234
13 .	1109	331	1038	1014	1052	514	1057	726	1055	703	1065	67
14		المعاللة	377	41000	911	46136	192	20826	93-	28005	857	1120
		58700		76150		8915C		50420		50000		5634

Figure 34. Input from Report DOT-HS-801:430 Variable Names and Density/Weight Values for Each Segment (Reference 9).

		TAGLE		AND CENTER	OF GRAVITY	luni15"		NSITY L	0000020
			DENSITY		MASS				
-		SEGME		MASS	7433	Aleste	Y Colie	- Lobe	وديوروب
								1	0000040
7		 _	-Levus	4541.4	9.41	1			7020250
9	2	2	1.000	50901.1	43.06	5	-1.1		3300000
4		3	بددنان	0174.2	10.04		1.0		3030070
4	4	4	1.000	1920.7	3.03	41.6	-5.4		000000
9	5	2	Ladiu	903.1	1.54	33.8	-4.4	5.4	JC076 40
ý	0	•	1.330	410.2	.00	33.3	4		0030100
4			1.000	2411.4	1.23	-23.0	-4.6	28.9	0000110
9	à	8	1.000	941.0	1.01	-31.0	-2.7	5.7	0000120
4	9	7	1.000	347.9	. 20	-14.5	.9		3000130
9	10	LJ	1.000	020009	9.93	12.0	1.0	-30.5	30001+0
9	- 11		1.000	2212.2	3.54	ló.l	2.2		0030150
4	14	12	1.000	311.5	1.30	47.5	4.4		001010
9	_13	_ 13	1.000	355.301	9.52	-10.4	1.4		JOSO 170
9	14	14	1.000	2234.0	3.53	-13.7	2.7		0030130
9			_1.000	111.0	1.23	-15.4	3.7		0000190
9	10	Lo	1.000	33075.3	53.90	4	7		0030230
	••	PARTS		330.3.3			-••	13.2	0300210
9	17	L	1.300	37710.3	600	5	4	19.7	0000220
9	_13	2	1.000	3360.0	5.28	25.7	-4.3		0000220
9	19	3	1.000	336/.1	5.29	-20.1	-3.2		
ý	20	4	1.000	9230.6	14.77				0000240
9	21	5					-4.0		ودعودوه
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9		WHOLE							0030270
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			4455	AND CENTER	OF GRAVITY	PZTIAUL			0003750
			DENSITY	MASS	MASS	A C.G.	Y C.G.	4 C.G.	
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21	1	L	1.000	4150.4	5.33		1.0	62.4	033780
21	- 2	_ 2	1.000	34001.5	44.47		-1.2		U003770
			1.000		10.37		.7		0003000
	3	3		8150.3		-11			
	3	3		8150.3					
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21 21	5 	<u>.</u> 	1.000	2:09.5 11:5:5 494.1	1.4d	34.5 42.4	-3.0 -2.4	36.a 4.9 -17.J	003620 003620 0003620
21 21 21 21	5 7	3 7	1.000	2:09.5 1103.0 494.1 2328.4	1.4d 1.4d .63 2.90	34.5 42.4 -24.1	-3.0 -2.4 -7.3	36.a 4.9 -17.d 33.5	0003a 10 0003a 26 0003a 20 0003a 40
21 21 21 21 21	5 -3 7 8	3 7	1.000 1.000 1.000 4.000 1.000	2:09.5 1105.5 494.1 2326.4 1100.0	2.63 1.43 63 2.90 1.47	34.5 42.4 -24.1 -30.1	-3.0 -2.4 -7.3 -5.3	36.a 4.9 -17.d 33.5	0003a . 0 0003a 2 0 0003a 2 0 0003a 4 0 0003a 5 0
21 21 21 21 21 21	5 3 7 8	7 A 9	1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2324.4 1100.0 422.0	2.63 1.43 -63 2.90 1.47	34.5 42.4 -24.4 -30.1 -41.1	-3.0 -2.4 -7.3 -3.3 -3.5	30.0 4.9 -17.1 33.5 -0.1	0003a 10 0003a 20 0003a 20 0003a 40 0003a 50 0003a 60
21 21 21 21 21 21 21 21	5 7 8 9	7 8 9	1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 7532.5	2.63 1.46 -63 2.50 1.47 -54 5.64	24.5 42.5 -24.1 -30.1 -41.1	-3.0 -2.7 -5.3 -3.8 5	36.a 4.9 -11.d 33.5 -0.1 -15.0	003a . 0 0003a 2 0 0003a 2 0 0003a 4 0 0003a 5 0 0003a 5 0 0003a 5 0
21 21 21 21 21 21 21 21 21	5 7 8 9	7 7 9	1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.0 494.1 2326.4 1100.0 422.0 7532.7 2027.0	2.6d 1.4d 6d 2.90 1.47 54 5.64	24.1 34.5 42.4 -24.1 -30.1 -41.1 11.9	-3.0 -2.4 -7.3 -3.3 -3.3 -3.4 -5.3 -4.2	36.a 4.9 -17.d 33.5 -0.1 -15.0 -31.5 -77.0	0034 - 00
21 21 21 21 21 21 21 21 21	5 7 8 9 10	7 7 9	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 7532.4 2067.0 1050.5	2.6d 1.4d .63 2.90 1.47 .54 5.64 3.07	14.5 42.4 -24.4 -30.1 -41.1 11.0 14.5	-3.0 -2.9 .7 -5.3 -3.8 5 1.7 4.2 9.2	36.0 4.9 -17.4 33.5 -0.1 -15.0 -31.5 -77.0 -169.9	0034 - 00034 -
21 21 21 21 21 21 21 21	5 7 8 9 10 11 12	7 7 4 9 11 12	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 7532.4 2087.0 1090.5	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39	24.3 34.5 42.4 -24.4 -30.1 -41.1 11.9 14.5 14.0	-3.0 -2.7 -7.3 -3.8	36.0 4.9 -17.0 33.5 5.1 -15.0 -21.5 -77.0 -169.9 -30.3	02-0000 04-0000 04-0000 04-0000 06-0000 07-0000 08-00000 08-0000 08
21 21 21 21 21 21 21 21 21 21 21 21 21 2	5 7 8 9 10 11 12 13	4 5 7 4 9 11 11 12 13	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.5 494.1 2324.4 1100.5 422.0 7532.4 2027.0 1050.5 5278.9	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52	24.3 34.5 42.4 -24.1 -30.1 -41.1 11.0 14.5 -40.7 -13.0	-3.0 -2.4 -7.3 -3.8	36.a 4.9 -17.u 33.5 -15.0 -17.u -109.y -30.3 -77.o	0.13×10 0.29500
21 21 21 21 21 21 21 21 21 21	5 7 8 9 10 11 12 13 14 15	4 5 7 4 9 11 11 12 13 14 15	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2169.5 1105.3 494.1 2324.4 1100.0 422.0 7532.3 2067.0 1050.5 0278.9 3010.1 1113.5	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52 3.83 1.42	14.5 -24.1 -24.1 -30.1 -41.1 11.9 14.5 -14.0 -10.7 -13.0	-3.0 -2.4 -7.3 -3.8 5 1.7 4.2 4.2 4.2 3.5 10.3	3G.a 4.9 -17.4 33.5 -15.0 -21.5 -77.6 -109.9 -30.3 -77.6 -110.2	20236 00386 003860 0038600 0038600 0038600 0038600 0038600 0038600 0038600 0038600 0038600 0038600
21 21 21 21 21 21 21 21	5 7 8 9 10 11 12 13	3 7 3 9 11 11 12 13 14	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.5 494.1 2324.4 1100.5 422.0 7532.4 2027.0 1050.5 5278.9	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52 3.83	24.3 34.5 42.4 -24.1 -30.1 -41.1 11.0 14.5 -40.7 -13.0	-3.0 -2.4 -7.3 -3.8	3G.a 4.9 -17.4 33.5 -15.0 -21.5 -77.6 -109.9 -30.3 -77.6 -110.2	0003a . 0000a . 0003a . 0000a . 0003a . 0000a
21 21 21 21 21 21 21 21 21	5 7 8 9 10 11 12 13 14 15	7 7 9 11 12 14 15 16 PARTS	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.0 494.1 2326.4 1100.0 422.0 75.32.7 2027.0 1090.5 0278.9 3010.1 1113.5 42837.9	2.6d 1.4d .6d 2.90 1.47 .54 5.64 3.67 1.39 10.52 3.8d 1.42 54.44	14.5 42.4 -24.1 -30.1 -41.1 11.0 14.5 14.0 -40.7 -13.0 -12.9	-3.0 -2.4 -7.3 -3.8 -5.3 -5.4 -5.2 -5.2 -5.2 -6.2 -7.4	36.a 4.9 -17.u 33.5 -15.0 -31.5 -77.u -169.9 -30.8 -77.0 -110.2 18.5	0033a . 00036
21 21 21 21 21 21 21 21 21 21 21 21	5 7 7 9 10 11 12 13 14 15 10	7 7 9 11 12 12 12 12 12 12 12 12 12 12 12 12	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 7532.7 2027.0 1050.5 0278.9 3010.1 1113.5 42837.9	2.6d 1.4d .63 2.90 1.47 .54 5.64 3.07 1.39 10.52 3.83 1.42 54.44	14.5 42.4 -24.1 -41.1 11.6 14.5 14.6 -13.0 -12.7	-3.0 -2.4 -5.3 -3.8 -3.8 -3.8 -3.8 -3.8 1.7 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2	3G.a 4.9 -17.4 33.5 -15.0 -21.5 -77.0 -10.9 -17.0 -110.2 18.2	0034 - 0000 00036 - 0000
21 21 21 21 21 21 21 21 21 21 21 21	5 7 7 9 10 11 12 13 14 15 10	4 5 7 7 8 9 11 11 12 13 14 15 15 14	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.5 494.1 2324.4 1100.0 422.0 7532.4 20278.9 3010.1 1113.5 42337.9 47,034.3 3709.4	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52 3.83 1.42 54.44	24.3 34.5 42.4 -24.1 -20.1 -41.1 11.0 14.5 14.0 -10.7 -13.0 -12.9	-3.0 -2.4 -5.3 -3.8 -5 1.7 4.2 9.2 1.4 3.5 10.3 -1.1	3G.a 4.9 -17.0 33.5 -15.0 -11.5 -77.0 -16.9 -17.0 -10.2 -18.2 -22.4 -16.4	0034 20 000 000 000 000 000 000 000 000 000
21 21 21 21 21 21 21 21 21 21 21 21 21 2	5 	7 7 3 9 11 12 14 15 14 15	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 75.32.5 2027.0 1050.5 9278.9 3010.1 1113.5 42837.9 47.034.3 37.09.4 3911.1	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52 3.83 1.42 54.44	14.5 -24.1 -24.1 -11.1 -41.1 -41.1 -40.7 -13.0 -12.9 -0	-3.0 -2.4 -5.3 -3.8 -5 1.7 4.2 4.2 3.5 10.3 -1.1	3G.a 4.9 -17.0 33.5 -15.0 -11.5 -77.0 -16.9 -17.0 -10.2 -18.2 -22.4 -16.4	0034 20 00036 20 00036 40 00036 00 00036 00 00036 10 00036 10 00037 10 00037 10 00037 10 00037 10 00037 10 00037 10
21 21 21 21 21 21 21 21 21 21 21	5 3 7 8 9 13 11 12 13 14 15 10 17 18 19 20	7 7 4 9 11 12 13 14 15 14 15 14 14 15 14 14 15 14 14 15 14 14 15 14 15 14 15 14 15 14 15 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 7532.3 2067.0 1050.5 9278.9 3010.1 1113.5 42337.9 47.034.3 3709.4 3911.1 11300.4	2.6d 1.4d .63 2.50 1.47 .54 5.04 3.07 1.39 10.52 3.83 1.42 54.44	14.5 -24.1 -24.1 -20.1 -41.1 11.9 14.5 -40.7 -13.0 -12.9 -0.7 -13.0 -12.9	-3.0 -2.4 -5.3 -3.8 -5 1.7 4.2 9.2 1.4 3.5 10.3 -1.1	3G.a 4.9 -17.4 33.5 -0.1 -15.0 -21.5 -77.0 -109.9 -30.3 -77.0 -110.2 18.2 -22.4 16.4 26.7 -50.3	00034 00 00034 00 00036 40 00036 40 00036 40 00036 40 00039 40 00039 40 00039 40 00039 40
21 21 21 21 21 21 21 21 21 21 21 21	5 	7 7 4 9 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 75.32.5 2027.0 1050.5 9278.9 3010.1 1113.5 42837.9 47.034.3 37.09.4 3911.1	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52 3.83 1.42 54.44	14.5 -24.1 -24.1 -11.1 -41.1 -41.1 -40.7 -13.0 -12.9 -0	-3.0 -2.4 -5.3 -3.8 -5 1.7 4.2 4.2 3.5 10.3 -1.1	3G.a 4.9 -17.4 33.5 -0.1 -15.0 -21.5 -77.0 -109.9 -30.3 -77.0 -110.2 18.2 -22.4 16.4 26.7 -50.3	00038-00 00038-00 00038-00 00038-00 00038-00 00038-00 00038-00 00038-00 00038-00 00038-00 00038-00
21 21 21 21 21 21 21 21 21 21 21	5 3 7 8 9 14 11 12 13 14 15 16 17 18 19 20	7 7 4 9 11 12 13 14 15 14 15 14 14 15 14 14 15 14 14 15 14 14 15 14 15 14 15 14 15 14 15 14 15 15 15 15 15 15 15 15 15 15 15 15 15	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2109.5 1105.3 494.1 2326.4 1100.0 422.0 7532.3 2067.0 1050.5 9278.9 3010.1 1113.5 42337.9 47.034.3 3709.4 3911.1 11300.4	2.6d 1.4d .63 2.90 1.47 .54 5.04 3.07 1.39 10.52 3.83 1.42 54.44 59.77 4.79 4.91 14.70	14.5 -24.1 -24.1 -20.1 -41.1 11.9 14.5 -40.7 -13.0 -12.9 -0.7 -13.0 -12.9	-3.0 -2.4 -5.3 -3.8 -5 1.7 4.2 9.2 10.3 -1.1 9 -2.5 5	3G.a 4.9 -17.4 33.5 -0.1 -15.0 -21.5 -77.0 -109.9 -30.3 -77.0 -110.2 18.2 -22.4 16.4 26.7 -50.3	0003a 00 0003a 00 0003a 00 0003a 00 0003a 10

Figure 35. First Two Tables of Herron's Data Input for HER1.

GR.	AVITY TAE	LES AITH DE	ENSITY=1.0		SS AND CENTER OF
THE HEW	WE IGHTS	WENE CALCUL	LATED FROM	THE DENSITY	- MEAN VALUES AND
	SCHOS 4	LUMES			
	DENSITY		HERREN'S	OLC	Něm
SUBJECT		DENSITY 4	JULUME	aE LOHT	#ELGHT
-	1.055u	0.9900	4041.0	4025.0	4079.7
,	1.366.1	4894	4196.4	4152aJ	4230.0
	Lacson	1.4591	4552.1	402100	4345.7
	1.0520	1.0340	3235.1	3456.0	3240.1
5	1.0550	C.GAS2	4154.0	4105.0	4194.3
	1.0300	8059.0	3517.5	3471.0	3551.3
THE HEAD		DENSI	TY 4 MEAN	VALUE IS 1	9a
	CENSITY		HERRONAS	al B	New
SUBJECT	CGT	JENSITY 4	VULUME	MEIGHT	WEIGHT
1	1.6676	0.9311	1926.7	1794.0	1764.4
2	1.0030	C. 9201	2109.5	1941.0	- 1531.8
3	0.9810	C.9187	2440.9	2246-0	2246.7
4	0.9330	0.3345	1730.8	1536.0	1592.3
5	1.0120	C. 9225	1907.4	1815.0	1801.6
6	3.9970	0.5174	1873.7	1715.0	1715.8
The k us	PPER ARM	DENSI		ALUE IS 0.9	
	DENSITY		1500 Out 6		
SUBJECT		DENSITY .	HERRON'S	OLC MELSHT	NEW AEIGHT
	1-401.1	1.0382	963.1	971-0	346.3
	1-0170	1.1391	1105.3	1293.0	1172.2
3	1.0350	C. 4904	1525.4	1024.0	103400
				756.C	
				.311.0	

Figure 36. HER1 Output.

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SECTION 6

THE AEROSPACE MEDICAL RESEARCH LABORATORY DATA BANK AND RELATED MATERIALS

Since the formulation of the AMRL Data Bank, five anthropometric data tapes have been documented and published in AMRL Technical Reports, several others are near publication form, and several programs are now being prepared for publication as AMRL Technical Reports. Two publications, referenced later in this section, have been submitted which fully document four anthropometric survey data tapes, and the correlation tape which contains correlation information for seven anthropometric surveys. Also two correlation tapes of a comparison format, each containing two groups of survey data, which were prepared independent of the AMRL Data Bank are described.

6.1 THE AMRL DATA BANK LIBRARY OF COMPUTER PROGRAMS

Work is progressing steadily on the library of computer programs. A large portion of the documentation has been written and several programs await final touchup, including the XVAL and MSDP programs. Work towards completion of this library is at this time picking up speed. The programs, with complete documentation, will be published during the coming year as part of an AMRL Technical Report.

6.2 THE AMRL DATA BANK TAPE LIBRARY

The standardization of the AMRL Data Bank Tape Library is progressing steadily. Five tapes have been fully documented and published in AMRL-TR-77-2 in September 1976 (see Reference 10). The first four tape volumes in the Technical Report contain the basic survey data from the four most important USAF anthropometric surveys: the 1950 and 1967 surveys of flying personnel, the 1968 survey of Air Force Women, and the 1965 survey of male personnel. The fifth tape is the tape of U.S. correlations which is documented in Paragraph 6.3 of this report.

6.2.1 Tape Format

Since the AMRL report on these tapes is rather complete, this report will only attempt to familiarize the reader with their basic format and content. These tapes have been prepared in essentially a common format for ease in their use not only in AMRL, but in research efforts elsewhere as well. All records on the tape are in 80-character card-image form. The tapes have been made relatively self-explanatory in as much as only one format statement to read in text and other format statements contained in the tape, need be supplied by the user. Each tape contains a heading record, an identification record, a small amount of historical background information on the data, coding information, data variable names, ranges, suitable interval widths for frequency tables, conversion factors for the data, and all but one format statement for reading the tape. Several relevant constants are also provided in the third record of each tape. Figures 37a-f show a listing of the first five subjects of the 1968 USAF female personnel survey tape. The text explaining the different sections of the tape is quoted directly from AMRL-TR-77-2.

6.2.2 Summary

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Since the publication of the AMRL Technical Report on the first five volumes of the Data Bank Tape library, nine other tapes are in nearstandard form, lacking only historical background and coding information. These nine and several others will be completed during the next contract period.

6.3 INTERCORRELATIONS OF ANTHROPOMETRIC MEASUREMENTS

Three correlation tapes have been prepared during the past year. Two of them have been comparison oriented tapes, each containing the information from two different correlation matrices. The third tape contains eleven files of correlation matrices based on data from seven large U.S. anthropometric surveys.

AMRL DATA BANK LIBRARY - VOLUME I - 1964 SURVEY OF AIR FORCE WOMEN

Line 1, as it appears, is simply the name of the survey. This is repeated as the last line of the tape heading so that it can be used as a heading for any output generated by the use of this tape.

. REC 0002.. 1619H .1411

> Line 2 is a format statement for reading in and writing out the next line.

REC 0803.. HSURVEY= 101; NVO = 140; NVT = 156; NSB = 1905; NLS = 47; NDATE = 7608

Line 3 provides several constants relevant to the contents of the tape: NSURVEY - an identifying number for the survey; here, NSURVEY=101

- the number of ordinal variables; NVØ=140. NVT - the total number of variables; NVT-156.

(Non-ordinal variables always follow the ordinal ones.) - the number of subjects; NSB=1905. NSB

- the number of lines of the description of the survey

and its coding: NLS=43.

NDATE - the date at which this tape was prepared; NDATE=7608, i.e., August 1976.

REC 0004.. (14,2x,2A9,3F8.2,2F6.2,2F10.7)
REC 0005.. (14,2x,3A6,3F8.2,2F6.2,2F10.7)
REC 0006.. (14,2x,4A4,A2,3F8.2,2F6.2,2F10.7)

THE PROPERTY OF

Lines 4, 5, and 6 are three alternate formats for use in reading in the name-range-conversion constant records. The first of these reads in the name as two 9-character words, the second as three 6character words, and the third a four 4-character and one 2-character words. The user of these tapes will presumably use the format most appropriate for his computer, or simply use the last of the three.

Figure 37a. The Heading and Identification Records and Some Formats (Reference 10).

The next several lines (i.e., NLSlines) are background material of some value, we hope, to the user of the tape's data but irrelevant to the computer's treatment of these data. The last of these NLSlines is a repeat of the initial line.

```
REC 0007.. THE SURVEY OF HOMEN OF THE AIR FORCE WAS HADE IN THE SPRING OF 1966 BY THE ANTH-
REC 0008.. ROPOLOGY BRANCH, AEROSPICS HOLICIAR RESEARCH LABORATORY, HAIGHT-PATTERSON AF8. O
REC 0009.. HIO AND THE ANTHROPOLOGY RESEARCH PROJECT (THEM AT ANTIOCH COLLEGE, YELLOW SPRING
REC 0010.. SO, OHIO). DATA FOR AGE (VARIBBLE 1), 123 BOOY SIZE HASDREHENIS VARIBBLES 2-12.
REC 0011.. 1, AND GRIP STREMENT (VARIBBLE 12), 123 BOOY SIZE HASDREHENIS VARIBBLES 2-12.
REC 0011.. 13 HEASUPENENTS HERE REPEATED ON 1513 SUBJECTS HITH THE SUBJECTS HEARING FOUNDA
REC 0012.. 13 HEASUPENENTS HERE REPEATED ON 1513 SUBJECTS HITH THE SUBJECTS HEARING FOUNDA
REC 0013.. 13 HEASUPENENTS HERE REPEATED ON 1513 SUBJECTS HITH THE SUBJECTS HEARING FOUNDA
REC 0014.. 1900) ARE RECORDED IN TENTHS OF FILL THE SUBJECTS HEARING FOUNDA
REC 0015.. 0 DECIPIS OF YEARS. SKINFOLOS ARE RECORDED IN TENTHS OF HILLTETES, WEIGHT AND
REC 0015.. 0 DECIPIS OF YEARS. SKINFOLOS ARE RECORDED IN THIS OF HILLTETES, WEIGHT AND
REC 0016.. HOUNDAIN OF YEARS. SKINFOLOS ARE RECORDED IN MILLIMETERS.
REC 0017.. HOUNDAIN OF THE RETIL VARIBBLES HERE RECORDED IN MILLIMETERS.
REC 0017.. HOUNDAIN OF THE RETIL VARIBBLES HERE RECORDED IN MILLIMETERS.
REC 0019.. AS REPORTED PLUS 0.5
REC 0019.. AS REPORTED PLUS 0.5
REC 0019.. AS REPORTED PLUS 0.5
REC 0012.. 11-FOUNDAITON GARNENT
REC 0012.. 11-FOUNDAITON GARNENT
REC 0012.. 11-FOUNDAITON GARNENT
REC 0012.. 11-SINGLE PROPER SPECIALTY CODE (SEE TAPE BOOKLET)
REC 0012.. 11-SINGLE PROPER SPECIALTY CODE (SEE TAPE BOOKLET)
REC 0012.. 11-SINGLE PROPER SPECIALTY CODE (SEE TAPE BOOKLET)
REC 0013.. 13-SINGLEAR PARTY CIRCLE PROPERTY / 7-HISCELLAMEOUS OR NOT SPECIFIED / 15-RANK
REC 0013.. 15-LT-COL / 36-COLONEL / 31-RANK / 13-SIRMAN / 13-SIRMA
```

Figure 37b. The Historical Background and Coding Information (Reference 10).

The following NVT (as read from line 3) lines provide information about each variable: names, ranges, conversion constants, and the like. This information can be ignored, in whole or part, by both the human users of these tapes and the computers. The I-th of these lines contains, in order:

I, (Name (I,L),L=1,NLGTH), (A(I,L),L=1,7)

where NIGTH is the length of the name in words. NIGTH depends on the computer word length and must be supplied by the user of the tape.

The quantities $\lambda(I,L)$ are these—we illustrate using the values for weight:

A(I,1)=82.50 a value slightly lower than the smallest value of weight recorded. This value was selected as an appropriate lower limit for the first interval when weights are grouped for frequency tables containing up to but not in excess of 50 intervals.

A(I,2)=200.00 the largest weight recorded.

A(I,3)=126.00 an approximation to the mean weight, included for use in reducing the size of summations of squares and higher powers.

A(I,4)=3.00 a suggested interval width for frequency tables which are limited to a maximum of 50 intervals. In this case, a table of 40 intervals will result; an interval of 2 pounds would have been too fine, and would have resulted in almost 60 intervals. Intervals for linear measurement have generally been restricted to values of 1, 2, 5, 10, 15 or 20 mm.

A(I,5)=5.00 a suggested interval width for frequency tables which are limited to a maximum of 30 intervals.

A(I,6)=0.4535924 a constant to convert the summary statistics from the units in which they were measured to the desired metric units for output. Here the conversion is from pounds to kilograms. Since the measurements are generally made in metric units, the function of A(I,6) is usually to adjust the location of the decimal point.

A(I,7)=2.2046223 a constant to convert the metric output to English units. For weight, this constant converts from kilograms back into pounds.

Figure 37c. The Variable Name-Range Records (Reference 10).

REC	0054	1 .	AGE	_18000	57500.	23444	1000	2000	_1000300	10000000
	0055	2	WEIGHT	8250	20000	12600	304	500	4535924	22046223
	0056	3	TRICEP" SKINFOLD	5250	46800	18000	1000	2000	103000	3937008
	9457	4	SUBSCAPULAR SKINFO.		37200	12000	1000	2000	100600	3937008
	0058	5	SUPHAILIAC SKINFLD	+250	50000	19000	1000	2006	100000	3937006
REC	0059	6	MEDIAL GALF SKINFO	1250	37200	15000	1600	2000		3937008
									103066	
REC	0060			144250	163000	162000	1000	2000	1000070	- 3937008
REC	0061	8	STATURE, MAXIMUM	144250	184000	162000	1000	2000	1000000	3937009
REC	0062	9	CERVICALE HEIGHT	120250	156800	139600	1000	2000	1000000	3977008
REC	0063	10	ACROMIAL HEIGHT	114250	152000	131000	1000	2000	1000000	3937008
REC	0064	11	SUPRASIERNALE HIGHT	116250	150600	131000	1060	2000	1000000	3937005
REC	0065	12	BUST POINT HEIGHT	100250	136303	115000	1000	2000	1000000	3937008
REC	C066	13	HAIST HEIGHT	86250	115500	100000	1000	2000	. 1003000	3937008
REC	0067	14	ABOOMINAL EXT HGT	78250	100000	93000	1000	2300	1000000	3937008
REC	0068	15	TROCHANTERIC HIGHT	68250	96500	82030	1000	2300	1000068	3937005
REC	0009	16	BUTTOCK HEIGHT	64250	96600	52000	1000	2000	_ 1000000	3937008
REC	0070	17	GLUTEAL FURROW HGT	58250	86430	72000	1000	2400	1000000	3937008
REC	0071	18	TIBIALE HEIGHT	33250	49600	41000	500	1000	1000000	3937008
REC	0072	19	CROTCH HEIGHT	60250	87500	74000	1000	2000	1000000	
REC	0073	20	ANKLE HEIGHT	7250	16030	11000	500	500	1000000	3937008
REC	0074	21	LAT"L HALLEOLUS HT	4750	8700	5700	500	500	1000000	3937008
	0075	22	SITTING HT, RELAXED	73250	96000	84000	500	1000	1000000	3937008
	0076	23	SITTING HEIGHT	75250	96400	85530	500	1000	1033330	3937006
	0077	24	EYE HEIGHT, SITTING	63253	83100	73600	560	1000	1003000	3937008
REC	0078	25	MIDSHOULDER HT,SIT	50250	67200	57600	500	1300	1033060	
REC	0079	26	HAIST HGHT, SITTING	17750	29200	23100	500	500	1000000	3937008
REC		27	ELOOM REST HEIGHT	14250	29500	22500	544	1000	1003000	3937008
REC	0081	28	POPLITEAL HEIGHT	. 33250		40 3 0 0	500			
REC	0082	29	BUTTOCK-POPLITTL L		47100				100,000	
				38250	58500	47600	500	1000	1000000	3937008
REC	0003	30	BUTTOCK-KNEE LNGTH	48250	60400	57200	500	1000	1000000	3937008
REC	0084	. 31	ACROMION-RADIALE L	25254	36500	30903	. 500			3937036
REC	0035	35	RADIALE-STYLION L	15750	28000	23200	500	500	1000000	3937008
REC	3086	13	THUMB-TIP REACH	65520	87200	74000	1000	1000	1000000	3977008
SEC	0087	34	THUMB-TIP, EXTENDED	_ 70250	100000	83000	1000			3937008
SEC	0088	35	OVERHEAD REACH	174250	227640	198000	1500	3000	1000000	3937003
REC	0089	36	NECK CIRCUMFERENCE	20250	39900	33600	500	530	1000000	3937008
REC	3090	37	SHOULDER CIRCUMFER		122100	103000	1000 .	2000	1000000	3937008
REC	0091	38	CHEST CIRC AT SCYE	70250	103500	84000	1000	2000	1000030	3937005
REC	0092	39	BUST CIRCUMFERENCE	74250	113900	89000	1000	2000	1007060	3937008
REC	0093	40.	CHEST C BELOW BUST	60250	97000	74000	1000	2000	1000000	3937005
REC	C094	41	WAIST CIRCUMFERNCE	52250	95100	67000	1000	2000	1000000	
REC	0095	42	ABOOM!"AL EXT CIRC	64250	119000	85500	1500	2500	1000000	3937008
REC	0096	43	HIP C-7"BLH HAIST	76250	117000	93000	1600			
REC	0097	44	HIP C-9""BLW WAIST	76250	120100	95000	1000	2000	1000030	
REC		45	UPPER THIGH CIRCUM	42250	72000	55000	1060	2000	1003000	
REC	0099	46	KNEE CIRCUMFERENCE	30250	45700	36000	500	1000	1000000	
	0100	47	CALF CIRCUM. RIGHT	26251	44500	3+040	500	1000	1000000	
	0101	48	CALF CIRCUM, LEFT	. 26250	44000		500			
REC		49	ANKLE CIRCUMFERNCE	17250	25600	34000		1000	1000000	
REC	0103	50	VERTICAL TRUNK CIR	134250		21000	544	500	1000000	
REC		51	VERTICAL TRK C,SIT	132250	178200	154000	1000	2000	1000000	
REC		52	BUTTOCK CIRC. SIT		170500	150000	1006	2000	1000000	
REC		53	SCYE GARGUMFERENCE	34250	128400	99000	1000	2000	1000000	
REC		54	AXILLARY ARM CIRC	28250	49000	37000	540	1000	1000000	3937008
REC	0107	55		20250	39100	27200	543		1000000	
REC			BICEPS C, RELAXED, R	19250	37400	25200	500	1000	1000000	
		56	BICEPS C.FLEXED: R	19250	39000	25400	500	1000	1000000	3937008
REC	0110	57	BICEPS C,RELAXED,L	19250	37800	25640	500		1000000	
REC		50	BICEPS C.FLEXED, L	19250	39200	25400	500	1040	1030000	
REC		59	ELSON CIRC, FLEXED	21250	35800	26700	500	1000	1003030	
REC		60	FOREARH C, RELAXED	19250	30000	23400	500	500	1000000	3937008
REC		61	FOREARM C, FLEXED	19250	32600	24900	540	1466	1000000	3937008
REC		62	WRIST CIRCUMFERNCE	12250	17600	14800	500	500	1000000	39 77008
REC		63	BIACROMIAL BREADTH	39750	41603	35700	500	500	1000000	
REC		64	BIDELTOID BREADTH	34250	50100	41700	540	1000	1000000	3937008
REC		65	CHEST BREADTH	22250	35900	27900	500	1000	1000000	3937008
REC		66	BUST PT-BUST PT BR	12750	24600	15300	500	500	1000000	3937008
REC		67	WAIST BREADTH	18250	32700	24000	500	1300	1000000	3937069
SEC		68	HIP BREADTH	28250	44100	34800	500	1000	1030000	
	0122	69	THIGH-THIGH BR, SIT	28253	50200	38000	560	1000	1003000	
REC	0123	70	HUMERAL BREADTH, R	5150	7500	6100	100	100	1000000	

Figure 37d. (Reference 10).

SEC	0124	71	HUMERAL BREADTH, L	5150	7400	5100	100	100	1000000 3937008
	0125	72	FEMORAL BREADTH, R	6650	9900	8100	200	200	1000020 _ 3937008
		73	FEMORAL BREADTH, L						
	0126			6653	9900	3100	500	590	1903000 3937008
	0127	74	CHEST DEPTH	18250	32303	23400	500	1000	1000000 3937004
SEC	0128	75		12251	25500	16800	500	1000	_ 1000000 3937004
REC	0129	76	ABOOMINAL EXT OPTH	15250	30300	20700	500	1000	1060000 3937.05
REC	0130	77	BUTTOCK DEPTH	15250	30600	21000	500	1000	1000000 3937008
	0131	78	THIGH CLEARANCE	5750	16900	12400	500	500	1000000 3937008
	0132	79		11250			500		
			SHOULDER LENGTH		18803	14600		500	1000000 3937009
	0133	40	NECK-BUST POINT L	19250	35000	25200	500	1000	1000000 3937005
KEC	0134	31	STRAP LENGTH	52250	79700	65000	1000	2000	1000030 3937003
REC	0135	92	INTERSCYE	27250	44200	34800	5.0	1040	1007000 3937406
REC	0136	83	INTERSCYE, MAXIMUM	37250	64500	49000	500	1000	1000000 3937008
REC		84	BACK CURVATURE	33250	53500	42430	500	1010	1001010 3937008
KEC	0138	85	WAIST BACK	33250	48100	43500	500	1000	1000000 3937008
	0139	16	ANTERIOR WAIST LTH	27250	41500	33300	500	1000	1000000 3937008
	3148	. 47	SLEEVE INSEAM	36250	53500	44000	500	1000	_ 1000000 _ 3937006
REC	0141	48	SPINE-TO-SCYE LGTH	15250	25500	20100	500	500	1000000 3937008
REC	0142	89	SPINE-TO-ELBON LTH	44250	62500	53200	Sud	1200	1000000 3937008
REC	0143	90	SPINE-TO-WRIST LTH	67250	91200	79500	500	1000	1000000 _ 3937008
	0144	91	HAND LENGTH	15250	22030	15200	200	500	
									1000000 3937008
	0145	92	HAND BREADTH	6450	8800	7500	100	200	1000000 3937009
REC	0146		HAND CIRCUMFERENCE				_ 500.	500	10000003937000
REC	0147	94	FOOT LENGTH	20750	27600	24000	500	540	1000000 3937008
REC	0148	95	FOOT BREADTH	6750	11000	3800	500	500	1000000 3937008
	0149	96	HEAD LENGTH		20700	18400	200		_ 1000000 3937000
	0150	17	HEAD BREADTH	12250	17100	14500	240		
								500	1000000 3937008
	0151	98	HEAD CIRCUMFERENCE	49750	61700	54600	500	500	1000000 3937008
REC	0152	99	TRAGION-TOP HEAD	10250	16100	12600	200	500	1000000 3937008
REC	0153	100	ECTOCANTHUS-TOP HO	8250	15700	11600	200	500	1030000 3937008
	0154		PRONASALE-TOP HEAD	10250	19300	14600	200	. 500	1000000 - 3937005
REC	0155		SUBNASALE-TOP HEAD	12250	20500	15800	200	500	1000000 3937008
	0156		STONION-TOP HEAD	14250	23100	17800	SúO	500	1000000 3937008
REC				18250				500	
REC	0158	105	TRAGION TO WALL	7250	14600	13000	200	500	1000000 3937003
REC	0159	106	ECTOCANTHUS-WALL	13250	21200	15200	200	500	1033060 3937008
REC	0160		PRONASALE TO HALL		25000		200		_ 1000000 3937008
	0161		SUBNASALE TO HALL	16250	24030	19600	200	530	1003000 3937409
	0162		LIP PROTRUS"N-WALL	16250	24100	19200	200	500	1000000 3937009
	0163			14250	22900	18200	200	. 500	1000000 3937006
	J164		SAGITTAL CURVATURE	29750	41500	34500	500	500	1003000 3937008
REC	0165	112	BITRAGION-CORONAL	23750	39200	33900	500	500	1000000 3937008
	0166		BIOCULAR BREADTH			. 9600		- 200	1030500 3937008
	0167		BIAURICULAR BROTH	13250	20100	15804	200	500	1000000 3937005
			BITRAGION BREADTH						
	3164			11250	15200	12800	200	200	1000000 3937008
	0169		BIZYGOMATIC BROTH		14900	12800		_ 200	1000000 3937008
	2170		BIGONIAL BREADTH	8450	12230	10100	200	200	1000000 3937008
REC	0171	118	NASAL BREADTH	2250	4600	3100	200	200	1003000 3937408
REC	0172	119	LIP LENGTH	. 3450	5800	4300	200	200	10000003937008
	0173		MENTON-SUBNASALE L	3850	7500	5500	100	200	1000000 3937008
	0174		MENTON-SELLION LTH	4650	12800	10600	100	200	1002000 3937009
	0175				6100	4500			
			SUBNASALE-SELLION				160	200	1000000 3937008
	0176		EAR LENGTH	3450	6940	5200	100	200	1030000 3937005
	0177		EAR BREADTH	1850	4200	2900	100	200	1000000 3937008
REC	0178	125	GRIP STRENGTH	950	. 5300	2904	100	200	13000000 3937305
REC	0179	126	WAIST HEIGHT, OFG	86250	115300	104000	1600	2000	1000000 3937008
	0180		ABOOM EXT HGT, OFG	78250	167900	95100	1000	2000	1000000 3937008
REC	0181		WAIST CIRCUM, OFG	54250	69000	66000	1600	2000	
REC			ABOOM EXT CIRC.OFG	64.250	146500				
	0132		AGOOM EXT CIRC, OFG	64250	118200	87000	1500	2500	1000000 3937008
REC	3183		HIP C-7 BLW W. OFG	76250	118800	93000	1004	2000	1003000 3937008
	0184			76250	120209	95000	1000	2000	1000000 3937006
REC	0165	132	WAIST BREADTH, OFG	17250	30800	21300	500	1000	1000036 3937008
	0186		HIP BREADTH, OFG	27250	42700	33600	500	1000	1000000 3937008
	0147			11250	24700	15600		1000	
									. 1000000 . 3937008
SEC	0188		ABOOM EXT OPTH, OFG	13250	30200	19600	500	1400	1000010 3937008
REC	0149		BUTTOCK DEPTH, OFG	16250	30400	21300	504	1000	1000000 3937008
REC	3190	137	BUTTOCK C, SIT, OFG .	82250	128840	99000	1000	2000	1000000 3937008
REC	0191		THI-THI BR.SIT.OFG	28250	48300	37200	500	1000	1000000 3937004
REC			STATURE REPORTED	5750	7440	5400	100	100	25400050 3937008
	0193			8150					
400		244		0.130	. 13500		- 304.	200	4535924 22046223

Figure 37e. (Reference 10).

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REC	0194	141	FOUNDATION GARMENT	50	900	300	100	100	10000000	10000000	
REC	0195	142	AFSC	8750	9912830	5558440	985003	396500	10003000	10000000	
REC	0196	143	RACE	_ 50	300	200	100	100	. 100000000.	10000000	
REC	3197	144	MARITAL STATUS	50	430	100	100	100	10000000	10000000	
REC	0198	145	RANK (NUMERICAL)	1050	3600	1700	100	200	16003000	10020000	
REC	0199	146	COMMAND	50	600	200	. 100	100	10000000	_10000000	
REC	0200	147	LOCATION	50	600	200	100	100	10000000	10000000	
REC	0201	148	SLOOD TYPE	. 50	400	200	100	100	10000000	10000000	
REC	0202	149	RH FACTOR	50	200	100	100	100	10000000	10900000	
	0203		HANDEDNESS	50	300	100	100	100	10000000	10000000	
	0204		BIRTHPLACE, SUBJECT	-50	14000	4400	_1000	_1000	10000000	10000000	
	0205		BIRTHPLACE, FATHER	-50	18000	4800	1000	1000	10000000	10000000	
	0206		BIRTHFLACE , MOTHER	-50		4800	1000	1000	10000000	10000600	
	0207		YEAR OF BIRTH	11500	50500	50500	1000	1000	13000030	_10000000	
	8050		AGE AT MENARCHE	8500		13000	500	540	1000000	10000000	
	6020		YEAR HEASURED	3900				100		10000000	
PEC	0210	114	19F4.0/2(20F4.0/).2(2			0F4.0/9F		. 0.F6.	0.8F2.4.5F	3. 0.F4.01	-

At the end of the list of name-range-conversion unit records is the format statement for reading in the data. While the data were written on the tape in integer format to save space, the format statement provided assumes that everything except the subject number is to be treated as floating decimal values. This format statement is, therefore, not suitable for listing data read from the tape.

This material is followed by the data. Each data record consisting of a subject number (increasing but not always consecutive) followed by NVT data values. The last data record is followed by a pseudo-data record for which the subject number is negative. Thus the user can read in all the data by reading the data for NSB subjects or by reading data until a negative subject number is sensed. Care should be taken in reading the data until an end of file (EGF) is sensed to insure that the pseudo-data record is not treated as a normal data record.

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REC 0211.. 1 285 112 124 78 86 150156715811315126912511130 928 058 778 763 675 406 703
REC 0212.. 120 65 835 855 722 573 234 204 389 459 536 108 238 729 9021886 345 966 793 905
REC 0213.. 749 642 846 842 947 524 357 326 130 21151061474 945 343 252 228 239 229 223 2231.
REC 0214.. 221228148161392276191233.33326 62 62 86 852518322719912014325764934862425 378
REC 0215.. 339439192532802169 74179230 361831625651401221521631822231806166209135195188 392
REC 0215.. 312 95 169 133 126 97 35 43 55 109 50 56 32 25 913 842 612 843 875 878
REC 0216.. 2 315 127 182 106 108 10816241641140613181012711791080 337 830 800 744 405 738
REC 0217.. 214 328 177 223 215 922 357 62 116 2 9754 2 132 2 5 4 2 1 9 9 93941256839
REC 0218.. 2 315 127 182 106 108 10816241641140613181012711791080 337 830 800 744 405 738
REC 02218.. 13 60 805 873 769 603 261 255 397 476 585 307 235 745 9301953 345 996 845 922
REC 02218.. 2 315 127 182 106 108 3158 333 332 1966161215271050 391 279 251 297 260 263 252
REC 02218.. 2 315 127 182 106 108 315 333 332 1966161215271050 391 279 251 297 260 263 252
REC 02218.. 2252371463504492841942393355412 55 55 80 80254170204239142164770657352471995 419
REC 02228.. 34 154214541081575 76171270 4618314453912317133144626091910171218202222184 355
REC 02228.. 325 94 166 125 111 93 33 46 57 106 51 53 34 32 947 926 637 830 946 946
REC 02228.. 226 358 168 204 244 986 399 64 122 2 9754 2 232 2 3 2 1 4 1 3 42 41361556839
REC 0225.. 3 455 166 126 244 986 399 64 122 2 9754 2 232 2 5 3 2 1 4 1 3 42 41361556839
REC 0225.. 3 4 455 166 126 244 986 399 64 122 2 9754 2 232 2 5 3 2 1 4 1 3 42 41361556539
REC 0225.. 3 1 457 106 132 133 111 12 2 42 54 108 46 60 35 33 969 902 718 806 911 997 816 0224. 326 327 326 681 271
REC 0226.. 325 354 3421221556018146 31.02242 87184150558312211114415016167205141164214196194184 37 37 REC 0227.. 811 747 900 925 913 925 350 333 331 195161718571011 391 295 296 271 18 806 911 990 970 18 806 911 990 970 18 806 911 990 970 18 806 911 990 970 18 806 911 990 970 18 806 911 970 970 970 970 970 970 970 970 970 97
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Figure 37f. The Subject Data Format and the Data Itself for the First Five Subjects (Reference 10).

6.3.1 Two Tapes for Comparison

The first two correlation tapes contain information from the 1968 USAF WOMEN survey versus 1967 USAF MEN survey, and from the 1965 USAF survey's black basic trainees versus white basic trainees. One hundred similar variables from the three surveys were chosen by Edmund Churchill of Webb Associates for the basis of these tapes. The first two records on the tape are 80-character card images and contain the formats needed for reading the tape. Header information is contained in the next three records which describe the layout of the variable names and statistical information. Original survey variable names are listed for each survey along with their survey numbers (SR NO), mean values for each variables (X-BAR), and standard deviations (SD). Both surveys are listed side-by-side, as shown in Figure 38, with the two right-most columns listing the arithmetic differences between X-BAR (DELTA XBAR) and SD(DELTA SD) for the two surveys for each variable. Following the variable names is a table, which is 22 card-image records long, which illustrates the layout of the correlations. The correlations for both surveys are listed in one 100X 100 element matrix. The diagonal elements of the matrix were all set to zero while the correlations of one survey occupy the upper right section of the matrix and those for the second survey the lower left section of the matrix. Figure 38 is a partial printout of the 1967 USAF MEN versus 1968 USAF WOMEN (WAF) tape. Thus far no analyses have been done using these two tapes.

6.3.2 U.S. Correlations

The third correlation tape of correlation matrices was documented and published in September 1976 in AMRL-TR-77-1 (see Referencell). The following is a portion of the abstract from that publication.

"Correlation matrices based on data from USAF anthropometric surveys of women (1968, 125 variables), flying personnel (1950, 128 variables; 1967, 190 variables), and basic trainees (1965, 161 variables); a U.S. Army survey of women separatees (1946, 60 variables); the Health Examination

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X-9AR 22, 92256 6, 45184 127, 24189 110, 32441 154, 41558 110, 32441 154, 41558 110, 32441 154, 41558 110, 415, 59104 1314, 60153 110, 415, 60, 01365 1113, 18793 1120, 01365 1121, 18793 1120, 01365 1121, 18793 1120, 01365 1121, 18793 1120, 01365 1121, 18793 1120, 01365 1121, 18793 1120, 18793 1120, 18793 113, 18793 113, 18793 114, 66119 127, 01462 137, 01462 13	02 02 03 04 04 04 04 04 04 04 04 04 04 04 04 04	NAME WEIGHT WEIGHT SKE TRICEPS-LANGE SKF SUNSCAP"R-LNGE SKF TRICEPS-LANGE SKF TRICEPS-LANGE SKF TRICEPS-LANGE TRICHT NIPPLE HEIGHT GLUTEAL FURROW HGT GLUTEAL FURROW HGT GLUTEAL FURROW HGT CROTCH HEIGHT ANKLE HEIGHT	1967 USAF ***C-BAR 30.02862 173.57594 62. 12.74211 NGE 13.65639 NGE 13.65639 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.53049 1773.5308 1773.18753 1773.18753	6.29563 21.41646 5.31204 5.31204 5.31204 103.36749 61.73432 61.73432 61.73432 61.73432 61.73432 61.73432 61.73432 61.4373 11.46657 43.8355 43.8355 43.84373 41.44373 41.44373 41.44373 41.44373 41.44373	NELTA X-91R -7.191R -7.191R -17.58230 117.58230 -114.92459 -152.49742 -132.03051 -132.03051 -132.03051 -132.03051 -132.03051 -105.7879 -75.65958 -75.65958 -75.65958 -75.65958	0E L 1
AGE	40040000000000000000000000000000000000	NAME ELE ELE ELE FRICEPS-LANGE (F SURSCAP"R-LNGE (F SURSILIAC-HN IGHT (STATURE) ROUTOALE HEIGHT PROMION HEIGHT IPPLE HEIGHT IPPLE HEIGHT ITST HT-OMPHALION OCHANIERION HGHT ITOCK HEIGHT UUTCAL FURRON HGT EE CIRC HEIGHT OUTCAL HEIGHT	X-BAR 30 02002 173.57594 12.74211 13.65639 242.16197 1773.51047 1452.19394 1452.19394 1452.19394 1452.19394 1452.19394 1152.19394 1152.19394 1162.1952 933.65283 137.18763 613.27388	6. 29563 21. 41646 5. 13204 5. 13204 10.3. 34579 61. 7. 3432 58. 12487 58. 12487 57. 48096 57. 48096 47. 11151 43. 83550 40. 04578 5. 42078 31. 170558	X-94R -7.10126 -145.29410 117.56230 117.56230 -114.92469 -126.70490 -133.93741 -109.40315 -109.40315 -109.40315 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090 -109.7090	15521 -43.14747 -43.14747 -43.14747 -13.254362 -2.93409 -1.69599 -2.12649 -2.12649 -2.12649 -1.16978 -1.16978 -1.16978
1 AGE 127.28189 1 L65656 2 WEISH 2 SUBSCAPULAR SKINFOLD 2 0.32441 2 SUBSCAPULAR SKINFOLD 2 0.32441 2 SUBSCAPULAR SKINFOLD 2 0.32465 3 SUP AAILIAC SKINFOLD 197.23465 6 GERUMAL HEIGHT 131.8.60153 9 SUP RASILEMALE HEIGHT 131.8.60153 1 MAI ST HEIGHT 131.8.60153 1 MAI ST HEIGHT 131.8.60153 1 GAOTCH HEIGHT 131.8.6019 1 GAOTCH HEIGHT 1 102.78740 1 44.90602 1 ROCHANNERIC HGHT 1 120.82467 1 GAOTCH HEIGHT 1 102.78740 1 44.90602 1 ROCHANNERIC HGHT 1 102.78740 1 44.90602 1 ROCHANNERIC HGHT 1 102.78740 1 40.90602 1 TROCHANNERIC HGHT 1 10.86719 1 13.64234 1 10.65001 1 10.6	10040000010040	IGHT (F TAICEPS-LANGE (F SURSCAP"R-LNGE (F SUPRAILIAC-HPN IIGHT (STATURE) RRVICALE HEIGHT RROHION HEIGHT PPRE HEIGHT IST HT-OMPHALION OCHANTERION HGHT IST HT-OMPHALION OCHANTERION HGHT OTOCK HEIGHT	30.02882 173.57594 12.73.57594 12.65639 242.16197 177.353049 1520.71547 1452.19394 1452.19394 1452.19394 1652.69108 1664.6958 1665.6958 1666.6958	6.29563 21.41646 5.33004 5.33004 103.36749 68.12432 58.12432 57.48096 57.291285 47.11151 43.46657 40.04578 41.46895 11.48895 54.2078 54.2078 31.70558	-7.10126 -17.92405 117.92409 114.924530 -14.92732 -128.49742 -133.69341 -132.03051 -132.03051 -132.03051 -132.03051 -132.05016 -75.06816 -75.06816 -75.06816 -75.06816	144611111111444
2 WEISHT SKINFOLD 190.32441 54.41558 50.03854 5.0850APULAR SKINFO 120.5941 54.47749 5.080APULAR SKINFO 120.5941 54.47749 5.080APULAR SKINFO 197.23465 70.12367 70.123	222222222222222222222222222222222222222	I GHT F TRICEPS-LANGE F SURSCAP'-LNGE F SURSCAP'-LNGE F SURSITIAC-HON I GHT (STATURE) I GHT (STATURE) I GHT (STATURE) PROMION HEIGHT PPLE HEIGHT I ST HT-OMPHALION OCHANIERION HGHT OTOCK HEIGHT	173.57594 12.76211 13.66339 242.16197 1773.53049 1520.74547 1452.19394 1452.9394 1652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11652.9310 11653.9310 11653.9310	21,41646 5,3304 5,3304 61,73432 61,73432 57,49096 57,49189 52,24976 47,11151 47,11151 47,400,04578 24,85706 41,44,995 5,42078 31,70558 31,70558	-45.29405 1177.50230 114.92745 -152.49742 -133.03051 -132.03051 -132.03051 -109.40315 -112.05.05045 -75.05016 -25.3044 -25.32044 -25.65024	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
3 TRICEPS SKINFOLD 4 SUBSCAPULAR SKINFD 5 STATURE 5 STATURE 6 STATURE 7 CERVICALE HEIGHT 1391.95748 9 SUPASTATRALL HGHT 1314.60053 10 BUST POINT HEIGHT 1314.60053 11 MAIST HEIGHT 1314.60053 12 SUPASTAR HEIGHT 1314.60053 13 SUPASTRANLE HGHT 1314.60053 14.6101EAL FURROH HGT 13 BUSTOCK HEIGHT 13 BUSTOCK HEIGHT 14 GLUTEAL FURROH HGT 15 TROCHAMEREL HGHT 16 CLUTEAL FURROH HGT 17 ANKLE HEIGHT 17 ANKLE HEIGHT 17 ANKLE HEIGHT 18 GROWN REST HEIGHT 18 GROWN	E 4 2 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4	FRICEPS-LANGE SURSCAP"R-LNGE (F SUPRALLIAC-HPN IIGHT (STATURE) RNICALE HEIGHT RNICALE HEIGHT RNICALE HEIGHT FPLE HEIGHT ITST HT-OMPHALION OCHANTERION HGHT ITST HT-OMPHALION UTCAL FURRON HGT IEE CIRC HEIGHT OCTCH HEIGHT	12.74211 242.16539 242.16539 1573.53049 1520.74547 1452.19394 1452.19394 1052.69108 1052.69108 1052.69108 1052.69108 1052.69108 1052.69108 1052.80108 1052.80108 1052.80108 1052.80108 1053	5,13204 103302 103302 6173432 50,12407 54,91265 57,48095 57,48095 57,11151 43,6657 43,6657 43,6657 43,6657 43,46657 44,477 4	177.56230 -144.92469 -144.92469 -152.49742 -133.59341 -133.59341 -133.69345 -165.05969 -76.66969 -76.66969 -76.66969 -76.66969	4 * W
SUBSCAPULAR SKINFD 128.59108 49.47749	480 C 0 6 0 1 0 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(F SURSCAP"R-LNGE (F SUPRAILIAC-HPN IIGHT (STATURE) RVICALE HEIGHT ROHION HEIGHT PRASTERNALE HGHT INCHENTERION HGHT OCHANTERION HGHT ITOCK HEIGHT UTCAL HEIGHT OUTCAL FURRON HGT EE CIRC HEIGHT OUTCAL HEIGHT OUTCH HEIGHT	13.66639 1773.53049 1520.74547 1452.19394 1452.19394 1452.04416 1292.69108 1292.69108 139.69036 939.69036 137.18763 70.39802 811.27908 137.18763 70.39802	5,33002 103,36749 61,7480 56,12487 57,48096 57,48096 57,21151 43,86557 40,04578 41,46895 11,46895 11,46895 5,42078 5,42078 31,70558	114, 92469 -128, 749742 -128, 749742 -133, 59341 -132, 03051 -102, 03051 -102, 06816 -75, 6595 -25, 32044 -25, 32044 -75, 62761	2 W 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
F SUPTAILIAG SKINFLD 197.23.65 70.12367 6 573 10 10 10 10 10 10 10 10 10 10 10 10 10	24222222	(F SUPRAILIAC-HPN TRUTAL HEIGHT ROHION HEIGHT PRASTERNALE HGHT PRASTERNALE HGHT INT HTOMPHALION OCHANTERION HGHT OTOCK HEIGHT OTOCK HEIGHT OTOCK HEIGHT HEIGHT HEIGHT HEIGHT HEIGHT	242,16197 1173,53049 11520,74547 1452,19394 11522,69106 1292,59106 1292,59106 1379,69136 911,27908 137,1875 137,1875 811,27908	103 36749 56.1.73432 56.1.73432 57.48096 57.91265 47.1151 43.46657 40.04578 24.8550 40.04578 54.2078 31.70558 31.70558	-44,92732 -126,49742 -133,59341 -132,03051 -109,40315 -109,40315 -109,40315 -109,40315 -109,40315 -109,40315 -109,70616 -25,32044 -25,32044 -25,32044 -25,43371	0.0000000000000000000000000000000000000
6 STATURE 7 GERVICALE HEIGHT 1391-95748 55-19079 8 ACROHILAL HEIGHT 1391-95748 55-19079 9 SUPARTERNALE HGHT 1193-18793 52-13736 11 MAIST HEIGHT 1193-18793 52-13736 12 BUST POINT HEIGHT 1193-18793 52-13736 13 BUST POINT HEIGHT 1193-18793 52-13736 14 GLUERL FURROH HGT 727-0040 39-61141 15 GAOTCH HEIGHT 727-0040 39-61141 15 GAOTCH HEIGHT 727-0040 39-61141 179 ALL HEIGHT 727-0040 39-61141 179 ALL HEIGHT 727-0040 39-61141 180590ULNE HEIGHT 77-0090 39-61141 20 EYE HEIGHT 77-0090 39-61141 21 MIDSHOULDER HISST 579-9958 8-6-61521 22 POPLITEAL HEIGHT 737-00402 26-53607 23 POPLITEAL HEIGHT 737-00402 27-6-61521 24 MUSSHOULDER HISST 579-9958 8-6-61521 25 GACRONION-RADIALE L 233-6667 13-6-019 26 MUTOCK-POPLIT" L 477-19709 27-5-6-5-6-6 27 RADIALE-STYLION L 233-6667 13-6-019 28 THU49-TIP REACH 74-13-39-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6	0 r 0 6 3 1 5 2 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	IGHT (STATURE) ROUTCALE HEIGHT ROHION HEIGHT PRASTERNALE HGHT IST HT-OMPHALION OCHANIERION HGHT OTOCK HEIGHT UTEAL FURROW HGT HEE GIRC HEIGHT ROTCH HEIGHT HEE HEIGHT	1773,53049 1550,74547 1452,19394 1452,59108 1164,8256 939,69136 911,27908 496,496 496,496 137,1876 137,1876 811,27908 137,1876 811,27908	61,73432 57,4837 57,4837 52,2497 52,2497 43,4657 43,4657 43,8355 40,0457 41,46,95 11,48895 5,4207 30,12741	-152.49742 -133.49349 -133.03051 -109.40315 -112.905045 -112.905016 -79.06916 -79.06916 -75.92044 -25.32044 -75.82761	2021101211101
7 CERVICALE HEIGHT 1391.97748 55.19079 8 ACRAHAL HEIGHT 1318.60053 54.79437 9 SUPPARTENALE HEIGHT 1318.60053 54.79437 10 SUPPARTENALE HGHT 1320.01365 53.01809 11 MAIST HEIGHT 106.7 149.6053 54.79437 12 ROCHAMTERIA 1193.18793 52.13736 14 GLUTEAL FURROH HGT 72.70040 39.61141 14 GLUTEAL FURROH HGT 72.70040 39.61141 15 TITIALE HEIGHT 745.0409 40.29395 17 ANKLE HEIGHT 745.0409 13.54234 19 SITTIAL HEIGHT 745.09946 30.5001 22 HIGHT ANTILL HGHT 77.10709 25.5807 23 FEEDOM REST HEIGHT 77.10709 27.5857 24 GUITOCK-POPLIT"L 477.10709 27.5857 25 GLBOW REST HEIGHT 7410.4745 19.655113 26 GACROHION-ROILE 233.86667 13.66019 27 RADALE-STYLION L 233.86667 13.66019 28 THUM9-TIP, REACH 7410.475, 19709 27.5857 29 THUM9-TIP, REACH 7410.475, 19.709 27.5857 29 THUM9-TIP, REACH 7410.475, 19.709 27.5857 29 THUM9-TIP, REACH 7410.4737 22.65447 31 SHOYLUFR CIRCUMFER 1004.12703 54.76655 34 UPP-ER THIGH CIRCUMFER 1004.12703 54.76655 35 CALF CIRCUMFERNCE 87.75381 12.88973 13.8667 14.8371 12.88973 13.867701 36 CALF CIRCUMFERNCE 87.75381 22.65447 37 WERTICAL TRUNK CIR 1544.2529 66.69405 14.8276 14.8376 14.8371 14	ree312234	RVICALE HEIGHT PROBLEM HEIGHT PROBLEM HEIGHT FPLE HEIGHT FPLE HEIGHT FOCH HEIGHT OCHANTERION HGHT JTTOCK HEIGHT LUTEAL FURRON HGT EE CIRC HEIGHT KLE HEIGHT	1520.74547 1452.19394 1292.594106 1292.59108 1064.62562 911.27908 911.27908 137.18763 70.39862 931.62783 8137.18763	50, 12407 54, 918096 54, 918096 52, 24976 43, 43, 46657 43, 46657 43, 46657 43, 46657 43, 46657 41, 44373 111, 46895 5, 42070 30, 12741	-120,70799 -133,59741 -133,59741 -109,40315 -162,03642 -179,06816 -79,06816 -79,06816 -79,06816 -79,06816 -79,06816 -79,06816 -79,06816 -75,08761 -75,08761	20110101110
8 ACRAHIAL HEIGHT 1318,60053 54,79437 9 SUP PASTEMALE HGHT 1320,01365 53,011899 10 BUDS TOOLNAME HGHT 1320,01365 53,011899 11 BUDS TOOLNAME HEIGHT 10C2,72441 42,67776 13 HG FOLDIER HEIGHT 10C2,72441 42,67776 13 HG FOLDIER HEIGHT 122,72441 42,67776 13 HG FOLDIER HEIGHT 1419,82467 23,76293 17 FOLDIER HEIGHT 1419,82467 23,76293 17 FOLDIER HEIGHT 1419,82467 23,76293 17 FOLDIER HEIGHT 1419,82467 24,623996 13,68667 23,76961 22 ELBON REST HEIGHT 27,7359 26,58103 26,58103 22 ELBON REST HEIGHT 27,70109 27,58567 23,8677 23,8667 23,8677 23,8667 23,8677 23,8667 23,8677 23,877	•• 212234	PRASTERNALE HGHT PRASTERNALE HGHT ILST HT-OHPHAION ROCHANTERION HGHT TITOCK HEIGHT UTEAL FURROW HGT REE CIRC HEIGHT ROTCH HEIGHT ROTCH HEIGHT ROTCH HEIGHT	1452.19394 1452.04416 1292.59108 1292.69108 11064.82582 931.1952 941.1952 137.1878 137.1876 931.82709 893.47833	57.48096 56.91285 57.91285 57.11151 43.46657 40.84578 54.64373 11.464373 11.464373 11.464373 11.464373 11.464373 11.464373	-133.59341 -132.03051 -103.03051 -62.03045 -112.96595 -75.66816 -76.65534 -105.77879 -25.32044 -25.32044 -75.82761	21.5.5.11.5.
9 SUPRASTERNAE HGHT 1320,01365 53,01809 10 BUST POINT HEIGHT 1193,18793 52,13736 11 MAIST HEIGHT 1193,18793 52,13736 12 TROCHANTERIC HGHT 826,72441 42,65776 13 BUTTOCK HEIGHT 822,12703 41,62904 14 GLUTEAL FURROW HGT 727,00440 94,29395 17 MAKLE HEIGHT 111,86119 13,54234 14 LATT WALLEGUUS HT 67,7350 40,29395 17 MAKLE HEIGHT 75,730,04462 30,50001 20 EYE HEIGHT 737,004462 30,50001 21 MIDSHOULDER HT,SIT 579,997638 26,56103 22 ELBOW REST HEIGHT 737,004462 30,50001 23 POPLITEAL HEIGHT 410,4745 18,60513 24 BUSTOCK-POPLITY L 477,20137 26,33893 25 ACRONION-RADIALE L 733,86657 13,60019 27 RADIALE-STYLION L 733,86657 13,60019 28 THU49-TIP, KATENDED 330,33176 49,63574 29 THU49-TIP, KATENDED 330,33176 49,63574 31 SHOJIUPER CIRCUMFERNCE 337,49344 16,76695 34 UPPER THIGH CIRCUM 554,75301 42,19422 35 CALF CIRCUMFERNCE 72,0320 56,6547 36 CALF CIRCUMFERNCE 72,0320 56,6547 37 ANKLE CIRCUMFERNCE 72,0320 56,6947 38 VERTICAL TRUNK CIR 1544,2529 66,69405 39 VERTICAL TRUNK CIR 1544,2529 66,69405 34 UPPER CIRCUMFERNCE 317,97046 22,86439 11 35 SHOJIUPER CIRCUMFERNCE 317,97046 22,86439 11 36 SCYS CIRCUMFERNCE 317,97046 22,86439 11 36 SCYS CIRCUMFERNCE 317,97041 22,93311 11 37 SHOJEN FILE STYLEN RC, SIT 1500,65924 66,69405 36 CALF CIRCUMFERNCE 317,97046 22,86439 11 37 SCYS CIRCUMFERNCE 3170,97046 170,97046 170,97046 170,97046 170,97047 170,970	621223	DPRASTERNALE HGHT IPPLE HEIGHT ILST HT-OMPHALION OCHANTERION HGHT JTOCK HEIGHT UTEAL FURRON HGT EE CIRC HEIGHT OTCH HEIGHT HEIGHT	1452.04416 1292.59106 1064.6582 939.69136 911.27818 496.4901 70.3982 931.8279 931.8279 891.8279 891.8279 893.8279	54,91285 52,24976 43,46657 43,8355 40,04578 24,6578 11,48895 5,42078 30,12741	-132.03051 -109.40315 -109.40315 -112.96595 -79.06016 -76.6594 -76.6594 -25.32044 -25.32044 -75.82701 -75.82701	
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12 TROCHANTERIC HGHT 826.72441 42.67776 13 BUITOCK HEIGHT 822.12703 41.62914 15 ITGLALE FURDH HGT 727.0040 40.29995 16 GAOTCH HEIGHT 727.0040 40.29995 17 ANKLE HEIGHT 11.06719 13.54234 14 ATTLE ALLEOLUS HT 67.73650 13.60801 20 EYE HTGHT 75.77.00462 30.56061 21 MIDGHOULDER HT, SITTING 737.00462 30.56061 22 ELDAN KEST HEIGHT 727.00442 24.61521 23 POPLITEAL HEIGHT 737.00442 24.61521 24 DUITOCK-POPLITY L 477.11709 27.56867 25 ACKUMION-RADIALE L 310.05932 16.25687 26 ACKUMION-RADIALE L 310.05932 16.25687 27 RADIAE-STYLLON L 77.11709 27.56867 28 THUMB-TIP REACH 741.3124 16.76641 29 THUMB-TIP ERCHENCE 337.49344 16.76641 31 SHOULDER CIRCUMFERINCE 37.49344 16.76641 32 CHEST CIRCUMFERINCE 37.49344 16.76691 34 UPPER THIGH CIRCUM 554.75301 42.19425 35 KNET CIRCUMFERINCE 572.03202 54.76685 34 UPPER THIGH CIRCUM 554.75301 22.46598 35 WERTICAL TRUNK CIR 154.2529 66.65405 36 WERTICAL TRUNK CIR 154.2529 66.66405 37 ANKLE CIRCUMFERINCE 370.97048 22.86439 11.6070507 41 SCY-S CIRCUMFERENCE 370.97048 22.86439 11.6070507 42 SICEPS GAELMED 756.75301 17.80701 11.446105050504 11.60707 11.607	3242	GH THE	939,6936 901,1952 901,1952 901,2790 496,48001 M50,8228 137,1876 70,32709 8931,8779	43 46657 40 0 4578 24, 85706 41 44373 41 11, 4885 5, 42078 31, 7055 27, 40611	-112.96595 -79.06816 -76.65946 -76.65534 -105.77879 -25.32044 -75.82761	. 5 . 4 . 4
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14 GLUTEAL FURRON HGT 727,00040 39,61141 15 TITGLE HEIGHT 745,04409 40,29395 17 ANKLE HEIGHT 111,06719 13,54234 18 LATTL MALLEOLUS HT 67,7365 5,07042 20 EVE HTIGHT 37,00462 30,60007 21 HIDSHOLDER HT,SIT 679,97636 26,51103 22 ELBON KEST HEIGHT 27,00142 24,61103 23 POPLITFAL HEIGHT 27,00109 27,56001 24 HUDSHOLDER HT,SIT 579,97636 26,51103 25 GLONN KEST HEIGHT 27,10709 27,5657 26 ACROMION-RADIALE L 310,05937 16,25607 27 ACCOMION-RADIALE L 310,05937 16,25607 28 THUMB-TIP REACH 741,314 38,7224 29 THUMB-TIP PREACH 741,314 16,7261 31 SHOYLUFR CIRCUMFERING 37,49344 16,7261 31 SHOYLUFR CIRCUMFERING 574,7931 92,7769 34 UPPSTICAL TRUNK CIR 1004,12703 51,38271 35 KNET CIRCUMFERING 574,7931 12,6695 34 UPPSTICAL TRUNK CIR 1544,22629 68,69405 35 VERTICAL TRUNK CIR 1544,22629 68,69405 36 VERTICAL TRUNK CIR 1544,22629 68,69405 37 ANKLE CIRCUMFERING 210,65934 12,65931 38 VERTICAL TRUNK CIR 1544,22629 68,69405 39 VERTICAL TRUNK CIR 1544,22629 68,69405 40 BUTCOK CIRC SIT 1500,65944 65,56654 41 SCY-S CIRCUMFERIOR 20,774101 22,93311 42 SICEPS GAELMED, R 267-94016 23,150-5444 4 ELGON CIRC, FLEXED 269,75430 17,8274	15	E E	611,27908 496,48001 157,18763 70,39882 931,62709 819,47833	40.04578 24.05706 41.44373 11.46895 5.42078 31.7754 27.40611	- 84.26968 - 76.65534 - 105.77879 - 25.32044 - 75.82761 - 75.82761	1112
15 TIGILALE HEIGHT 749,82467 23,76293 16 GAOTCH HEIGHT 749,82467 23,76293 16 ANKLE HEIGHT 74,80719 13,54234 18 LAT"L MALLEOLUS HT 67,7395 9,9248 31,6807 20 EYE HIGHT, SITTING 737,04462 30,56061 21 HIDSHOLLDER HT, SIT 737,04462 30,56061 22 ELBDM REST HEIGHT 737,04462 30,56061 23 POPLITEAL HEIGHT 74,77,1079 27,56567 25 ACROMION-RADIALE L 37,6019 27,56567 25 ACROMION-RADIALE L 37,6019 27,2613 26 ACROMION-RADIALE L 33,6667 13,6019 27 HUM9-ITP REACH 741,31234 38,76264 29 THUM9-ITP REACH 741,31234 38,76264 29 THUM9-ITP REACH 741,31234 38,76269 30 NGCK CIRCUMFER UNG 74,72703 51,7519 31 SHOULEP CIRCUMFER UNG 554,75381 42,7659 34 UPP STRICAL TRUNK CIR 194,2703 54,76695 35 CALF CIRCUMFERNCE 73,311,4577 22,6947 36 CALF CIRCUMFERNCE 73,01470 22,6947 37 NAKE CIRCUMFERNCE 73,01470 22,6947 38 VERTICAL TRUNK CIR 194,2629 68,69406 39 VERTICAL TRUNK CIR 194,2629 68,69406 40 SUTTOCK CIRCUMFERNCE 770,97848 22,86439 11 44 ELBOM CIRC, FLEXEO 769,7810 17,87217	15	EH :	496.48001 A50.82288 137.18763 70.39882 931.82709 809.47833	24.85706 41.44373 11.48895 5.42078 31.70558 30.1274	-76.65534 -105.77879 -25.32044 -2.66024 -75.82761	112.1
16 GROTCH HEIGHT 145,04409 40,29395 17 ANKLE HEIGHT 11,86119 13,54244 19 SITTING HEIGHT 67,73619 5,67244 19 SITTING HEIGHT 67,7369 5,67014 20 EYE HEIGHT 73,714462 30,56001 21 HIDSHOULDER H1,511 579,97638 26,58103 22 ELDSHOULDER H1,511 579,97638 26,58103 23 DOPLITEAL HEIGHT 410,47454 18,60513 24 DUITOCK-ROPELIT'L 47,710709 27,56567 25 ACNOTALE-STYLION C 73,033,8667 13,60019 27 ACOTAL-STYLION C 73,8667 13,60019 28 THUMB-TIP REACH 741,3124 16,72613 29 NFCK CIRCUMFERINGE 377,49344 16,72643 31 SHOULDER CIRCUMFER 1004,12703 51,38271 32 CHEST CIRCUMFERINGE 377,49344 16,72691 33 KNET CIRCUMFERINGE 377,49344 16,72691 34 UPPER THIGH CIRCUM 554,75301 42,19425 35 CALF CIRCUMFERINGE 210,89339 12,88937 13 36 VERTICAL TRUNK CIR 1544,2559 66,64405 37 VERTICAL TRUNK CIR 1544,2573 60,88691 38 VERTICAL TRUNK CIR 1544,2529 66,64405 38 VERTICAL TRUNK CIR 1544,2529 66,64405 39 VERTICAL TRUNK CIR 1544,2629 66,64405 31 SCY-S CIRCUMFERINGE 210,89339 12,88937 11 31 SCY-S CIRCUMFERENCE 370,97048 22,88439 11 31 SCY-S CIRCUMFERENCE 370,97048 22,88439 11 31 SCY-S CIRCUMFERENCE 269,75430 17,80704 11 34 AND SCY-S CIRCUMFERENCE 370,94016 23,8311 11 34 AND SCY-S CIRCUMFERENCE 370,94018 22,88439 11 34 AND SCY-S CIRCUMFERENCE 370,94018 22,88439 11 35 SCY-S CIRCUMFERENCE 370,94018 22,88439 11 36 SCY-S CALER CONTRIBUTE 370,94018 22,88439 11 37 SCY-S CIRCUMFERENCE 269,75430 17,80704 11			450.62288 137.18763 70.39882 931.62709 8 99.47833	41.44373 11.48895 5.42678 31.70558 30.12741 27.40611	-105.77879 -25.32044 -2.66024 -75.82761 -72.43371	2
17 ANKLE HEIGHT 111.86719 13.54234 14 LAT"L MALLEOLUS HT 65.73858 5.70142 20 EYE HTIGHT 65.99948 31.68007 21 HIDSHOULDER HT.SIT 579.97638 26.58103 22 ELBOM REST HEIGHT 227.04462 30.56001 23 HIDSHOULDER HT.SIT 579.97638 26.58103 24 GUITOCK-POPLIT"L 477.11709 27.58567 25 GUITOCK-NEE LNGTH 547.28137 26.28567 27 AADIAL-STYLION L 233.86667 13.68019 28 THU49-TIP ERACH 741.31234 16.76571 29 THU40-TIP, EXTENDED 938.33176 49.77919 30 NCC CIRCUPFERNE 377.49344 16.76671 31 SHOULDER CIRCUPFER 1004.12703 51.38271 32 CHEST CIRCUPFERNE 573.646976 49.655574 34 UPP-ER THIGH CIRCUPFERNE 573.01470 22.65447 35 CALF CIRCUPFERNCE 573.01470 22.65447 36 CALF CIRCUPFERNCE 573.01470 22.65447 37 VERTICAL TRUNK CIR 1544.26299 68.69405 38 VERTICAL TRUNK CIR 1544.26299 68.69405 38 VERTICAL TRUNK CIR 1544.26299 68.69405 39 VERTICAL TRUNK CIR 1544.26299 68.69405 31 SCY-CIRCUPFERENCE 77.01709 22.65447 31 SCY-CIRCUPFERENCE 77.01709 22.65447 32 CALF CIRCUPFERENCE 77.01709 22.65447 33 VERTICAL TRUNK SIT 150.065949 65.69405 34 VERTICAL TRUNK SIT 150.065949 65.69405 37 VERTICAL TRUNK CIR 1544.26299 68.69405 38 VERTICAL TRUNK SIT 150.065949 65.69405 38 VERTICAL TRUNK SIT 150.065949 65.69405 38 VERTICAL TRUNK SIT 150.065949 65.69405 39 VERTICAL TRUNK SIT 150.065949 65.69405 37 VERTICAL TRUNK SIT 150.065949 65.69405 38 VERTICAL TRUNK SIT 150.065949 65.69405 37 VERTICAL TRUNK SIT 150.0659496 65.69405	26 16 C		137.18763 70.39882 931.82709 8 99.47833	11.48895 5.42078 31.70558 30.12741 27.40611	-25.32044 -2.66024 -75.82761 -72.43371	2
18 LAI"L MALLEOLUS HT 67,73650 5,87042 19 SITTING HEIGHT 855,99948 31,68807 21 MIDSHOULDER HT,SIT 879,97638 26,56103 22 ELBDM REST HEIGHT 227,00462 16,60513 22 ELBDM REST HEIGHT 227,004764 18,60513 24 BUTOCK-NOPLIT"L 477,10709 26,56103 25 ACKUMION-RADIALE 1310,85657 13,68019 26 ACKUMION-RADIALE 1310,85657 13,68019 27 HU49-TIP REACH 741,31234 38,7264 29 THU49-TIP,8 KTEACH 741,31234 38,7264 31 SHO'LUER CIRCUMFER 1004,12703 51,38274 31 SHO'LUER CIRCUMFER 1004,12703 51,38274 32 CHEST CIRCUMFER 1004,12703 51,38274 33 KNET CIRCUMFER 1004,12703 51,38274 34 UPPETICAL TRUNK CIR 1544,26299 68,69405 35 CALE CIRCUMFERNCE 210,8973 12,8673 36 CALE CIRCUMFERNCE 210,8973 12,8673 37 WERTICAL TRUNK CIR 1544,26299 68,69405 38 VERTICAL TRUNK CIR 1544,26299 68,69405 39 VERTICAL TRUNK CIR 1544,26299 68,69405 40 BUTTOCK CIPC, SIT 150,65946 65,56054 44 ELBOM CIRC, FLEKKO 269,74301 27,15675 CIRCUMFERENCE 370,94016 22,15454 44 ELBOM CIRC, FLEKKO 269,74301 27,15675 CIRCUMFERENCE 370,94016 23,11544 44 ELBOM CIRC, FLEKKO 269,7430			70.39662 931.62709 8 09.47833	5.42078 31.70558 30.12741 27.40611	-2.66024 -75.82761 -72.43371	
19 SITTHG HEIGHT 655.9946 31.60807 20 EYE HEIGHT, SITTING 737.04462 30.59081 21 HIDSHOULDER HT, SITTING 737.04462 30.59081 22 ELBOW REST HEIGHT 227.06142 24.61551 23 POPLITEAL HEIGHT 410.47454 18.60513 24 GUITOCK-NOPLITYL 477.19709 27.58657 25 ACROHION-RADIALE L 310.05932 16.25687 27 RADIAGE-TIP REACH 744.31234 38.77264 28 THU49-TIP REACH 744.31234 38.772919 30 N=CK CIRCUMFERENCE 337.49344 16.76571 31 SHOULDER CIRCUMFER 100.412703 51.38271 32 CHEST CIRCUMFERENCE 337.49344 22.19422 33 UPPER THIGH CIRCUM 554.75381 42.19422 34 UPPER THIGH CIRCUM 554.75381 42.19422 35 KNET CIRCUMFERENCE 341.43570 22.46598 37 ANKLE CIRCUMFERENCE 210.85939 12.88973 38 VERTICAL TRUK C.SIT 15.00.65944 65.5605447 41 SCY± CIRCUMFERENCE 370.97848 22.86439 42 SICEPS GARLAXEO, R. 267.94916 22.86439 44 ELBOW CIRC. REXCOL 756.7391 17.82747		LAT"L MALLEOLUS HI	931.62709	30.12741	-75.62761	-
20 EYE HEIGHT, SITTING 737,04462 30,56001 21 HIDSHOLLDER H1, SIT 579,97638 26,56103 22 ELDSHOLLDER H1, SIT 579,97638 26,56103 23 POPLITEAL HEIGHT 227,0462 24,61521 24 PUTTOCK-POPLIT" L 477,19709 27,55567 25 ACNUMON-RADIALE L 310,0532 16,25687 27 AADIALE-STYLION L 233,8667 13,68019 28 THUM9-TIP PEACH 74,3124 38,7264 29 THUM9-TIP, EXTENDED 337,4934 16,76671 31 SHOYLLFR CIRCUMFERINCE 377,4934 16,76671 31 SHOYLLFR CIRCUMFERINCE 377,4934 16,76671 32 CHEST CIRC AT SCY. 84,4937 51,38271 33 VERTICAL TRUNK CIR 341,4937 22,46596 34 UPP-IR THIGH CIRCUM 554,75381 42,1942 35 ANETICAL TRUNK CIR 1544,2629 68,6445 36 VERTICAL TRUNK CIR 1544,2629 68,6445 37 VERTICAL TRUNK CIR 1544,2629 68,6445 38 VERTICAL TRUNK CIR 1544,2629 68,6445 39 VERTICAL TRUNK CIR 1544,2629 68,6445 41 SCY- CIRCUMFERENCE 370,97848 22,88439 11 42 SICEPS CALEKEO, R 267,94016 23,15544 11 44 ELBOH CIRC, FLEXEO 78 26,7430 17,82741	19	SITTING HEIGHT	8 19.47 833	30.12741	-72,43371	
22 MIDSHOLLDER H1, SIT 579,97638 26,54103 22 ELBON KEST HEGHT 227,00142 24,65521 24 DIVIDICK-POPLIT"L 477,10709 27,56567 25 ACKUMION-RADIALE 1310,05937 26,33893 26 ACKUMION-RADIALE 1310,05937 16,25607 27 ACKUMION-RADIALE 1310,05937 16,25607 28 THU4B-TIP REACH 741,334 38,7264 30 NGCK CTRCUMFERNCE 37,4934 16,76671 31 SHOYLUFF CIRCUMFER 1004,12703 51,38271 32 CHETI CIRCUMFERNCE 672,0320 54,76605 34 UPPATICAL TRUNK CIR 14,4357 22,46591 35 KNET CIRCUMFERNCE 672,73381 42,1942 36 CALF CIRCUMFERNCE 73,01470 22,66447 37 NETICAL TRUNK CIR 1544,2629 68,69405 38 VERTICAL TRUNK CIR 1544,2629 68,69405 39 VERTICAL TRUNK CIR 1544,2629 68,69405 40 SCY± CIRCUMFERNCE 770,97848 22,88439 11 42 SICEPS GAELAKED, R 256,11391 22,93311 44 ELBON CIRC, FLEXEO 78 265,7430 17,86747	20	EYE HEIGHT/SITTING		27.40611		. 45340
22 ELBJM REST HEIGHT 227.06142 24.61521 23 POPLITEAL HEIGHT 477.1914 18.60513 25 DUITOCK-NOFILTUL 477.1917 27.56567 25 DUITOCK-KNFE LNGTH 574.20137 26.33893 26 ACRUMION-RADIALE L 310.05932 16.25607 27 RADIALE-STYLION L 233.86667 13.66119 28 THU49-TIP EXTENDED 838.33176 48.77219 30 NECK CTACUHFERENCE 337.49344 16.76214 31 SHOYLUF CIRCUMFERINCE 37.49344 16.76614 31 SHOYLUF CIRCUMFERINCE 672.03202 54.76685 34 UPP-ST THIGH CIRCUMFERINCE 672.03202 54.76685 35 MAIST CIRCUMFERINCE 672.03202 54.76685 36 CALF CTACUMFERINCE 672.03202 54.76685 37 ANKLE CIRCUMFERINCE 210.85939 12.88973 13 38 VERTICAL TRUNK CIR 1544.26299 68.659465 39 VERTICAL TRUNK CIR 1544.26299 68.659465 40 BUTOCK CIRCUMFERENCE 370.97848 22.86493 11 42 SICEPS G.FLEKEO, R 267.1391 22.93311 11 44 ELBOW CIRC, FLEXEO 269.75430 17.82747 11		MIDSHOUL DER HT/SIT	645.93774		-65.96136	82508
23 POPLIFEL HEIGHT 410.47454 18.65513 24 9UITOCK-ROPLITIL 477.10709 27.56567 25 ACRUMION-RADIALE L 310.05932 16.25667 27 RADIALE—STYLION L 233.6667 13.60019 28 THUMB-TIP REACH 741.31234 16.256019 30 N=CK CIRCUMFERNCE 337.49344 16.766119 31 SHOULDER CIRCUMFER 1004.12703 51.38271 32 CHEST CIRCUMFERNCE 337.49344 16.76671 33 N=CK CIRCUMFERNCE 37.49344 16.76671 34 UPPER THIGH CIRCUM 554.75301 42.19422 35 KNET CIRCUMFERNCE 672.03202 54.76685 34 UPPER THIGH CIRCUM 554.75301 22.65547 35 KNET CIRCUMFERNCE 10.65934 12.88977 13.41.45973 12.669105 37 ANKLE CIRCUMFERNCE 210.65934 65.56547 41 SCY± CIRCUMFERNCE 370.97048 22.86593 11.6704 CIRCUMFERNCE 370.97048 22.86593 11.6705 CAPLERED, R 267.11391 22.93311 14.4 ELGOM CIRC, FLEXED 269.75430 17.82747 11.143 11.672707	36 22 €1	ELBOW REST HGT/SIT	251.63904	26.07191	-24.57762	-1.45670
24 9UITOCK-ROPLITT L 477.19709 27.59567 25 ACKUNION-RADIALE L 310.99332 16.25687 27 AADIALE-STYLION L 233.86667 13.68019 28 THUMB-TIP PEACH 741.3124 38.72664 29 THUMM-TIP, EXTENDED 838.31376 48.77219 30 NCK CIRCUMFERINGE 337.4934 16.76611 31 SHO'LLPF CIPCUMFER 1004.12703 51.38771 32 CHEST CIRCUMFERINGE 672.03202 54.76685 34 UPP-ER THIGH CIRCUM 554.75381 42.19422 35 KNET CIRCUMFERINGE 573.0202 54.76685 34 UPP-ER THIGH CIRCUM 554.75381 42.1942 35 KNET CIRCUMFERINGE 210.8933 12.88937 31 VERTICAL TRUNK CIR 1544.26299 68.69465 33 VERTICAL TRUNK CIR 1544.26299 68.69465 41 SCY-L CIRCUMFERINGE 210.89339 12.88937 42 SICCPS GAELARED, 256.11391 22.93311 44 ELBOH CIRCL SEE		POPLITEAL HGHT/SIT	437.07404	22.40403	-26.59940	-3.79891
25 DUITOCK-KNEE LNGTH 574,20137 26,33893 26 ACRUMION-RADIALE 1310,05932 16,25607 27 RADIALE-STYLION L 733,66657 13,66019 28 THU48-TIP PEACH 741,31234 38,76264 29 THU48-TIP PEACH 741,31234 38,76264 31 SHOYLUFP CIRCUHFER LU04,12703 51,38271 32 CHEST CIRCUHFER LU04,12703 51,38271 33 MAIST CIRCUHFER LOT 672,0320 54,76695 34 UPPER THIGH CIRCUH 554,73381 42,19427 35 KNET CIRCUHFERNCE 73,01470 22,6547 36 CALF CIRCUHFERNCE 73,01470 22,6547 37 ANKLE CIRCUHFERNCE 10,6593 12,8693 12,8693 13,09716 CIRCUHFERNCE 10,65924 65,669405 38 VERTICAL TRUNK CIR 1544,2629 68,69405 39 VERTICAL TRUNK CIR 1544,2629 68,69405 41 SCY- CIRCUHFERNCE 770,97848 22,8653 14,4557 14,6917 15,67247 11,144 6LGOM CIRC, FLEXEO 76,7410 17,82747 11,144 6LGOM CIRC, FLEXEO 769,7410 17,82747 11,44	54	BUTTOCK-POPLITEAL	503.83845	25.73078	-26,73136	1.85489
26 ACROMION-RADIALE L 310,105932 16,25607 27 ALOIRION-RADIALE L 310,105932 16,25607 27 ALOIRION-L 233,86667 13,68019 27 HUMB-TIP EXTENDED 838,33176 40,77919 30 NECK CIRCUHFERINCE 337,49344 16,77671 31 SHOULDER CIRCUHFER 1004,12703 51,3871 32 CHST CIRC AT SCYE 842,4976 49,63574 33 MAIST CIRCUHFERNCE 672,03202 54,7668 34 UPP-ER THIGH CIRCUHFERNCE 672,03202 54,7668 34 UPP-ER THIGH CIRCUHFERNCE 210,8573 22,4659 37 ANKLE CIRCUHFERNCE 210,8573 12,88973 13 ANKLE CIRCUHFERNCE 210,8573 12,88973 13 ANKLE CIRCUHFERNCE 210,8573 12,88973 13 ANKLE CIRCUHFERNCE 210,8573 60,68945 37 VERTICAL TRK C,SIT 1500,65944 65,56945 41 SCY± CIRCUHFERNCE 370,97048 22,86493 14 SCY± CIRCUHFERNCE 370,97048 22,86499 14 EL90H CIRC, SIT 267,94016 23,15954 11 44 EL90H CIRC, FLEXED 269,75430 17,82747 11		BUTTOCK-KNEE LNGTH	604.12157	26.97580	-29.84021	63687
27 RADIALE-STYLION L 233.86657 13.60019 28 THUMG-TIP FREACH 741.3124 48.77219 30 N=CK CIACUMFERENCE 337.49344 16.76571 31 SHOULDER CIRCUMFER 1004.12703 51.38271 32 CHEST CIRCUMFERENCE 672.03202 64.76605 34 UPPER THIGH CIRCUM 554.75381 42.19422 35 KNET CIRCUMFERENCE 672.03202 54.76605 35 WERT CIRCUMFERENCE 573.01470 22.65647 36 ANKLE CIRCUMFERENCE 510.65939 12.66593 37 ANKLE CIRCUMFERENCE 210.65939 12.66593 38 VERTICAL TRUNK CIR 1544.26299 68.669405 39 VERTICAL TRUNK CIR 1540.26299 68.669405 41 SCY± CIRCUMFERENCE 370.97040 22.86693 42 SICEPS G.FELRKEO, R 267.1391 22.93311 11 44 ELGOM CIRC, FLEXEO 269.75430 17.82747 11	43 26 AC	ACROMION-RADIALE L	329.47244	17.00262	-19.41312	74575
29 THUMB-TIP PEACH 741.3124 38.7264 29 THUMM-TIP, EXTENDED 0308.33176 40.77919 30 NCK CIRCUMFERINCE 337.4934 16.76611 31 SHO'LLPF CIPCUMFER 1004.12703 51.38771 32 CHEST CIRC AT SCYF 642.49376 49.6374 34 UPP-IR THIGH CIRCUM 554.75301 42.19422 35 KNET CIRCUMFERINCE 572.03202 54.76695 35 KNET CIRCUMFERINCE 573.01070 22.65447 36 CALF CIRCUMFERINCE 310.8933 12.86937 37 VERTICAL TRUNK CIR 1544.26299 68.69465 39 VERTICAL TRUNK CIR 1544.26299 68.69465 40 BUITOCK CIRCL SIT 150.65944 65.56654 41 SCY-CIRCUMFERINCE 370.97848 22.86439 11.8782 60.86607 42 SIC-PS GARLAKED, R 267.94016 23.15954 11.8782 60.86607 44 ELBOH CIRCL FEXEO R 267.94016 23.15954 11.8782 60.86607 44 ELBOH CIRCL FEXEO R 267.94016 23.15954 11.8782 60.86607		RADIALE-STYLION LH	268.83635	14.20863	-34.96968	52845
29 THUM9-ITP, EXTENDED 838.33176 48.77919 30 NECK CIRCUMFERENCE 337.49344 16.72671 31 SHOULDER CIRCUMFER 1004.1270 3 51.38671 32 CHEST CIRCUMFERNCE 672.49376 49.65574 33 MAIST CIRCUMFERNCE 672.49376 49.65574 34 UPP.SE THIGH CIRCUM 554.75381 42.1942 35 KMET CIRCUMFERNCE 73.01470 22.65447 36 CALF CIRCUMFERNCE 303.01470 22.65447 37 ANNEE CIRCUMFRENCE 210.5933 12.8673 13.4847 39 VERTICAL TRUNK CIR 1544.26299 68.69405 39 VERTICAL TRUNK CIR 1544.26299 68.69405 41 SCY-E CIRCUMFERNCE 370.97848 22.86549 42 91C-PS G-RELAKED, R 255.11391 22.93311 11 44 ELBOM CIRC, FLEXED 269.75430 17.82747 11		THUMB-TIP REACH	A03.15986	39.75051	-61.84752	98787
30 NECK CIRCUHFERENCE 377.4934, 16.76671 31 SHOTLER CIRCUHFER 1004.12703 51.38271 33 SHOTLER CIRCUHFER 1004.12703 51.38271 33 MAIST CIRCUHFERNCE 672.03202 54.76685 34 UPP-ER THIGH CIRCUH 554.75301 42.19422 35 KMET CIRCUHFERENCE 576.01470 22.65447 35 KMET CIRCUHFERENCE 210.8573 12.88973 37 ANKLE CIRCUHFERNCE 210.8573 12.88973 38 VERTICAL TRUNK CIR 1544.26299 68.69405 39 VERTICAL TRUNK CIR 1564.26299 68.69405 40 89170CK CIRCUHFERENCE 370.97848 22.86493 11 41 SCY± CIRCUHFERENCE 370.97848 22.86493 11 42 BICEPS G,FLEKEO, R 267.11391 22.93311 44 ELBOH GIRC, FLEKEO, R 267.94016 23.15954 11	62	THUMB-IIP R"CH/XTD	895.94194	45.15364	-57.61018	3.62554
31 SHOULDER CIRCUHER 1004,12703 51,38271 32 CHE3T CIRC AT SCYE 842,48976 49,63574 34 MIST CIRCUHERNCE 672,93202 54,76685 34 UPPER THIGH CIRCUM 554,75381 42,19422 35 KNEE CIRCUHERNCE 34,143570 22,46594 37 ANKE CIRCUHERNCE 210,85039 12,86973 34 VERTICAL TRUK C,SIT 1570,65944 65,56054 41 SCYE CIRCUHERNCE 310,999,97333 60,86905 41 SCYE CIRCUHERNCE 370,97848 22,86433 42 SICEPS GARLAXED,R 256,11391 22,93311 44 ELBOM CIRC,R 226,75430 17,82747	30	NECK CIRC -MAXIMUM	393.42406	19.12700	-45.93062	-2.36029
32 CHEST CIRC AT SCYE 842,48976 49,63574 34 MAIST CIRCUMFERNCE 672,03202 54,76685 35 KNET CIRCUMFERNCE 672,03202 54,76685 36 CALF CIRCUHFERNCE 763,01470 22,65447 36 CALF CIRCUHFERNCE 210,8973 12,689405 39 VERTICAL TRUNK CIR 1544,26299 68,69405 39 VERTICAL TRUNK CIR 1544,26299 68,69405 40 BUITOCK CIRC, SIT 150,65946 65,69405 41 SCY± CIRCUHFERENCE 370,97323 60,88607 42 91C=PS GARLAXED,R 256,11391 22,93311 43 91C=PS GARLAXED,R 265,11391 22,93311 44 ELBOM CIRC, FLEXKO 266,76430 17,82747	31	SHOULDER CIRCUM"CE	1176.91249.	58.07640	-172,78546	-6.69369
33 HAIST CRCUMFERNCE 672,03202 54,76685 34 UPPER THIGH CIRCUM 554,75361 42,19422 35 KNET CIRCUMFERNCE 53,01470 22,65447 36 CALF CIRCUMFERNCE 210,8573 12,86973 34 VERTICAL TRUNK CIR 1544,26299 68,69405 34 VERTICAL TRUNK C,SIT 1500,65964 65,56054 40 BUTTOCK CIRC, SIT 999,97323 60.86607 41 SCY± CIRCUMFERENCE 370,97640 22,86439 42 91C5PS G,RELAXEO,R 265,11391 22,93311 44 ELBOM CIRC, RESKO 266,76430 17,82747	32	CHEST CIRC AT SCYE	1022.47917	69.56760	-179.98941	-10.93185
34 UPP_SR THISH CIRCUM 554,75381 42.19422 35 KNET CIRCUMFERENCE 363,01470 22.65447 36 CALF CIRCUMFERENCE 210.8573 12.46598 37 ANKLE CIRCUMFERNCE 210.8573 12.86973 38 VERTICAL TRUNK CIR 1544,26299 68.69405 39 VERTICAL TRUNK CIR 1544,26299 68.69405 41 SCY± CIRCUMFERENCE 370.97848 22.86439 42 91C FR CALAXED, R 267,1391 22.98431 43 BICCEPS GAELAXED, R 267,94016 23.15454 44 ELBOW CIRC, FLEXCO 269,76430 17.82747	33	WAIST CIR-OMPHAL"N	875.95456	73.67513	-203.92254	-18.90928
35 KNET CIRCUMFERINCE 53.01470 22.465447 36 CALF CIACUUM, RIGHT 341.43570 22.46598 36 VERTICAL TRUNK CIR 1544.26299 68.69405 37 VERTICAL TRUNK CIR 1544.26299 68.69405 39 VERTICAL TRUNK CIR 1544.26299 68.69405 41 SCY- CIRCUMFERENCE 370.97383 60.86607 41 SCY- CIRCUMFERENCE 370.97383 60.86607 42 91C-PS GARLAXED, R 256.11391 22.93311 43 91C-PS GARLAXED, R 267.94016 23.15454 44 EL90 WCIRC, FLEXKO 268.76430 17.82707	34	UPPER THIGH CIRCUM	588.15313	44.32350	-33,39932	-2.12928
36 CALF CIRCUM, RIGHT 341,43573 22,46598 37 ANKLE CIRCUMFIRNCE 210,85039 12,88973 39 VERTICAL TRUNK CIR 1544,26299 66,69405 39 VERTICAL TRUNK C.SIT 1560,65964 65,56054 40 GUITOCK CIRC, SIT 999,97323 60,86607 41 SCY- CIRCUMFIRENCE 370,97846 22,98439 42 91C-PS G.RELAXEO,R 267,94016 23,15454 44 E.BOW CIRC, FLEXEO 26,76430 17,82747	35	KNEE CIRCUMFERINCE	386.74716	20.74432	-23.73246	1.91015
37 ANKLE CIRCUMFERNCE 210.85039 12.88973 34 VERTICAL TRUNK CIR 1544.26299 68.69405 39 VERTICAL TRUNK C, SIT 1500.6594 65.56054 40 BUTTOCK CIRC, SIT 999.97323 60.88607 41 SCY± CIRCUMFERENCE 370.97640 22.86439 42 91C FPS C, RELAXED, R 265.11391 22.93311 44 BLOOM CIRC, FLEXCO 269.76430 17.82747	36	CALF CIRCUMF/RIGHT	371.91418	22.73158	-30.47848	26560
33 VERTICAL TRUNK CIR 1544,26299 68.69405 39 VERTICAL IRK C.511 1500.65946 65.6054 41 SCY- CIRCUMFERENCE 370,97848 22.86439 42 SIC-PS G-RELAXED, R 265,11391 22.98311 43 DIC-PS G-RELAXED, R 265,11391 22.93311 44 ELBOM CIRC, FLEXEO 269,7549016 23.15454	37	ANKLE CIRCUMF" LNCF	224.10112	12.64359	-13.24973	. 24614
39 VERTICAL IRK C.SIT 1500.65964 65.56054 40 BUTTOCK CIFC, SIT 999.97323 60.86607 41 SCY- CIRCUMFRENCE 370.97848 22.86439 42 91CEPS G.RELARCD,R 256.11391 22.93311 44 BIGGES G.FLEKED, R 267.94016 23.15454 44 ELBOW CIRC, FLEXED 266.76430 17.82747	38	VERTICAL TRUNK CIR	1680.66849	71.57992	-135.40550	-2.8858
40 BUTTOCK CIFC, SIT 999,97323 60.88607 41 SCY- CIRCUMFERRACT 370,97846 22.86439 42 SIC-PS G.RELAKED,R 256,11391 22.93311 44 B.DG-PS G.FLEKED, R 267,94016 23.15454 44 E.BOW CIRC, FLEKED 269,76430 17.82707	39	VERT TRUNK CIR/SIT	1613.05888	69.43687	-112, 39904	-3.8763
41 SCY± CIRCUMFERENCE 370,97646 22.86439 42 91CEPS GAELAXED,R 256,11391 22.93311 43 81CEPS G.FEKTO,R 267,94016 23.15454 44 ELBOM CIRC, FLEXED 269,76430 17.82707	73 40 01	BUTTOCK CIRCUM/SIT	1076.30121	67.24665	-76.32798	-6.35998
42 91C3PS G, RELAXED, R 256.11391 22.93311 43 D1C3PS G, FLEXED, R 267.94016 23.15454 44 ELBOW GIRG, FLEXED 269.76430 17.82707	103 41 SC	SCY CIRCUMFERENCE	483.60959	27.76742	-112.63111	-4. 88243
43 BIGEPS C,FLEXEO, R 267.94016 23.15454 1 44 ELBOW CIRC, FLEXED 269.76430 17.82707 1		BICEPS C-EXTENDIRT	307.81321	23.34424	-51.63930	41113
44 ELBON CIRC, FLEXED 269.76430 17.82707	43	BICEPS C-FLEXED/RI	327.41691	22.57789	-59.47675	. 57666
	17	FIRM CIRC-FLEXED	312, 39293	17.45950	-42.62863	36756
45 FORTARM C. RELAXED 234.76379 17.78454	45	LOWFR ARM C-EXTEND	291.52797	14.61580	-46.76419	83126
46 FOR ARM C. ELEVED 249.75066 15.10602	1		207 67106	15. 80570	-47.92730	KARTI

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9, 22987 19, 41351 25, 61348 23, 82119 21, 82119 18, 83757 18, 83757 16, 98757 16, 98757	34, 11433 17, 6254 30, 17511 23, 74216 23, 74216 26, 16635 35, 19134 6, 19629 9, 38321 11, 89037 4, 74466	5,41646 14,25937 7,019917 7,70147 11,02870 10,26629 10,24193 6,49766	7.49986 7.89880 8.5613 10.46713 12.84923 12.84915 6.07816 6.07816 7.55189 7.26796 6.08862 3.74275 3.72202 3.72202 3.72202
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	124, 36273 146, 60787 1493, 91341 405, 11181 441, 27192 203, 64182 775, 83832 775, 83832 775, 83832 175, 8418 183, 18085 240, 68609 64, 61612	145.15433 548.65459 117.25144 117.6477 147.60525 159.12369 119.07034 101.72441	2211,88871 196,62415 196,62415 186,53333 347,85984 347,85984 349,2257 34,78478 54,78478 55,41207 52,41207 29,81207
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Figure 38 (Continued)

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.03459 .03664 .00952 .06943	.46763 .42210 .80773 .29826 .10325	.08543 .05804 .058948 .014114	.05640 .06377 .48377 .03401	.14430 .06254 .47941 .03632 .01943
.01015 - 00606 - 13128 - 17057 - 09513 - 14638	.43258 .43258 .57218 .55276 .14543	.05135 .08429 .30068 .29427 .01341	.01399 .04586 .28025 .32436 .01964	.10534 .29850 .33108 .02650
.03874 .29278 .19376 .06056	.49651 .37595 .80540 .53411 .16778	.02317 .69185 .39182 .02191	.02641 .00204 .60581 .36359 .01224	. 10973 . 03790 . 56502 . 34007 . 01190
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.04811 .04566 - .27232 .11505 .00664	.53251 .16027 .78718 .48686 .39260	.09677 .41102 .28181 .05525	.00605 .03968 .37461 .20569 .04061	.09785 .07105 .35684 .23979 .06587
.01056 .13417 .02349 .13712 .05550	.58295 .49730 .59125 .53821 .51002	.60431 .14680 .31959 .20218 .05225	.09443 .17579 .11843 .03845	.11976 .22552 .19738 .10115
.16119 .10888 .04740 .19438 .13752 .06907	.56456 .44781 .75241 .77036 .49499	.61048 .11153 .48769 .52971 .15427 .06427	.02025 .34277 .42513 .12404 .12086	.68515 .09649 .37484 .44394 .16836 .10456
.14773 .09088 .14510 .14615 .13986	.99666 .48131 .81940 .76760 .41710	56406 . 10451 . 56406 . 46907 . 05736	. 57469 . 02599 . 41022 . 53533 . 04552	.67542 .08956 .44330 .57276 .98400 .11372
.22300 .00222 .15469 .23148 .38318		.53395 0 .08378 .63300 .40163 .09324		
	•	.16887 -54177 -52916 -13281 -09226		

Figure 38 (Continued)

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Survey of civilian adults (1960-1962, 20 variables); and a survey of law enforcement officers (1974, 23 variables) are presented for the use by engineers who need them in solving design problems and by anthropologists and statisticians, whose analyses and understanding of the interrelationships of body size data depend significantly on these coefficients. Sample sizes in these surveys ranged from 2000 upward..."

Ten correlation matrices are included on the tape, four from the Health Examination Survey of civilian adults and one each from the remaining six surveys. Matrices were produced one at a time on separate tapes and then merged into one eleven-file tape. The first file is a table of contents and includes a routine for abstracting data from the tape. Paul Kikta of UDRI is directly responsible for the programming runs needed to produce the matrices and the final tape, as well as the table of confidence limits included in AMRL-TR-77-1.

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